

# Extensive wind tunnel measurements to explore the conditional expected load method

Nicolas Blaise, Thomas Andrianne, Vincent Denoël

University of Liège (Belgium)

7th European-African Conference on Wind Engineering

EACWE 2017  
4-7 JULY 2017, LIÈGE

# Context

Le Nouveau Vélodrome Marseille



Stade de Lille Métropole

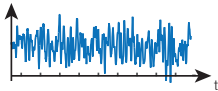


→ Equivalent Static Wind Loads?

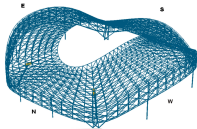
<complex structure, load combination, codification, simplicity>

# Equivalent Static Wind Loads

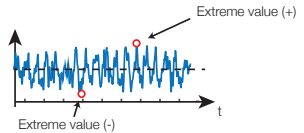
Wind pressure



Structural system

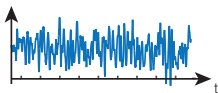


Structural response

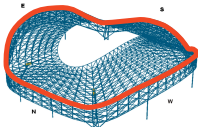


# Equivalent Static Wind Loads

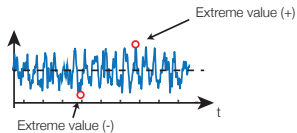
Wind pressure



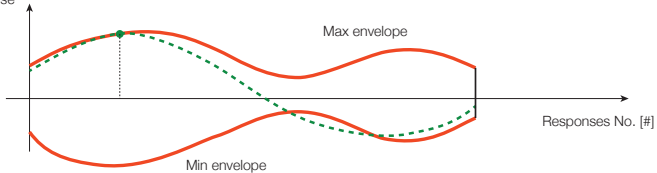
Structural system



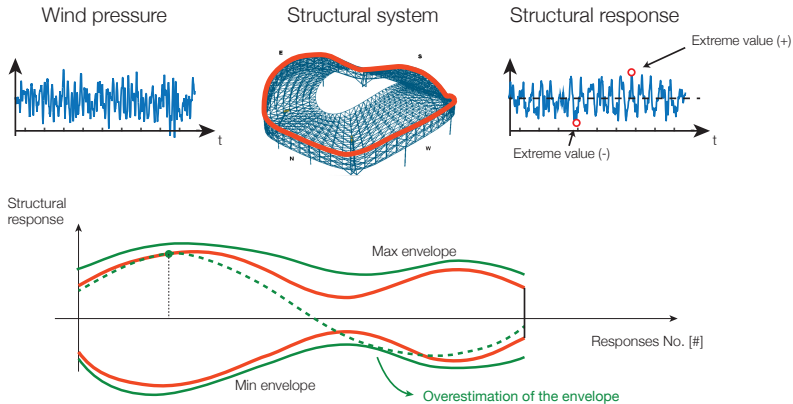
Structural response



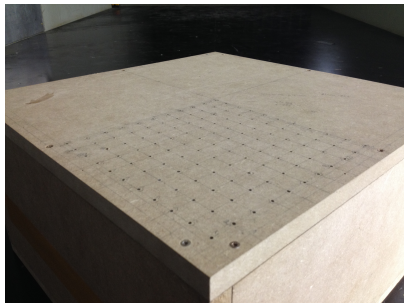
Structural response



# Equivalent Static Wind Loads



# Academic Example

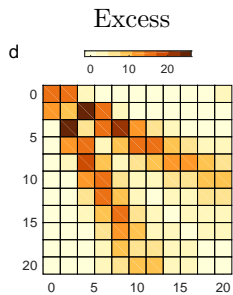
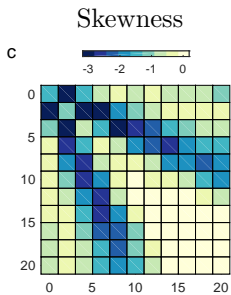
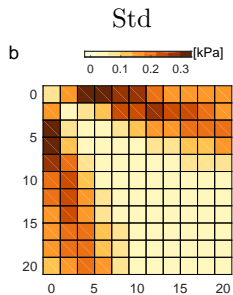
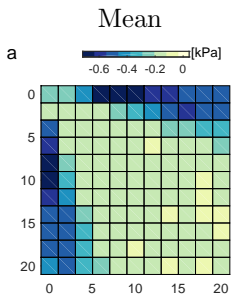


- ▷ Well-known wind pressure field
- ▷ Limitations of existing ESWLs
- ▷ Linear & static structural behaviour <simple enough>

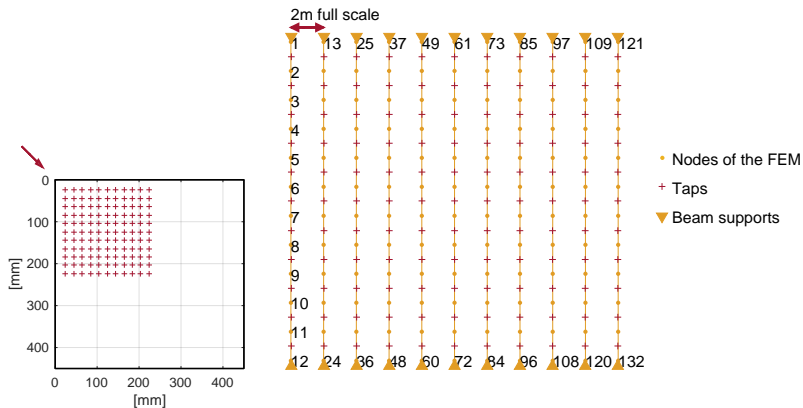


Non Gaussian pressure field !

# Pressure Field

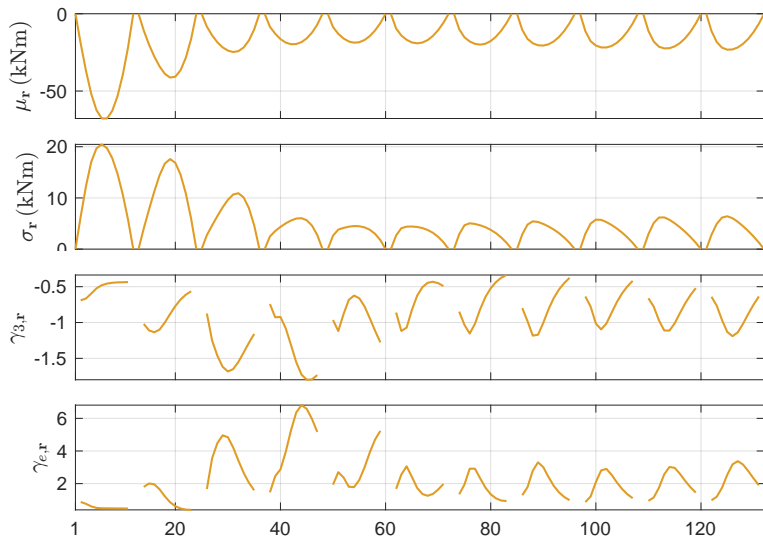


# Structural System



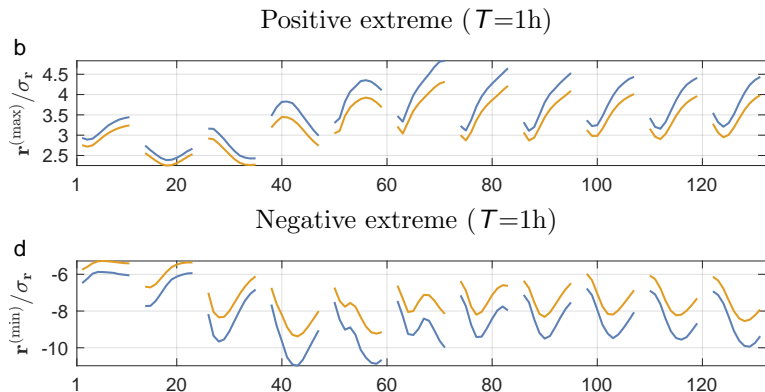


# Structural System: Bending Moments



Non Gaussian structural responses!

# Structural System: Bending Moments



Extreme values (Kareem-Zhao formula)

Mean extreme, 86% quantile for  $T=1$ hour

# Equivalent Static Wind Load

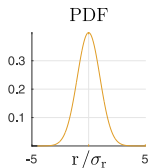
▷ Load-Response Correlation (LRC) [Kasperski 1992]

$$p = g\rho_{pr}\sigma_p$$

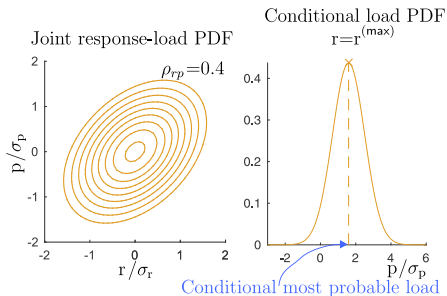
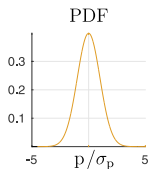
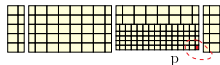


Gaussian context: **Most probable** extreme load pattern

Bending moment  $r=r^{(\max)}$



Aerodynamic pressure p



# Equivalent Static Wind Load

▷ Load-Response Correlation (LRC) [Kasperski 1992]

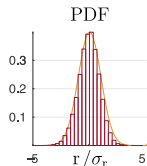
$$p = g\rho_p r \sigma_p$$



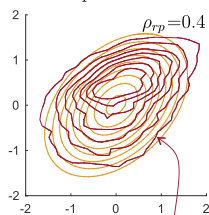
Non-Gaussian context: **No interpretation**

Bending moment  $r = r^{(\max)}$

$$\gamma_3 = -0.16, \gamma_e = 0.36$$

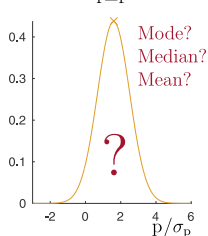


Joint response-load PDF



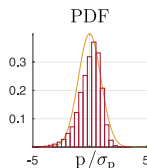
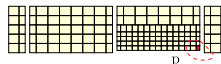
Conditional load PDF

$$r = r^{(\max)}$$



Aerodynamic pressure  $p$

$$\gamma_3 = -1, \gamma_e = 2$$



Kernel density estimation

# Equivalent Static Wind Load

- ▷ Conditional expected static wind load [Blaise et al., 2016]

$$p = \mathbb{E} \left[ p | r = r^{(\max)} \right] = \int_{\mathbb{R}} p \psi_{p|r} \left( p, r^{(\max)} \right) dp$$



Non-Gaussian context: conditional average of the pressures

- ▷ Bicubic Model (7-parameter)

$$p = g(u) = \frac{\alpha_u}{b_u} \left( \frac{u^3}{3} + a_u u^2 + (b_u - 1)u - a_u \right) \quad r = h(v) = \frac{\alpha_v}{b_v} \left( \frac{v^3}{3} + a_v v^2 + (b_v - 1)v - a_v \right)$$

$\alpha_u, b_u, a_u$ : Match  $\sigma_p$ ,  $\gamma_{3,p}$  and  $\gamma_{e,p}$

$\alpha_v, b_v, a_v$ : Match  $\sigma_r$ ,  $\gamma_{3,r}$  and  $\gamma_{e,r}$

$\rho_{uv}$ : Match correlation coefficient  $\rho_{rp}$

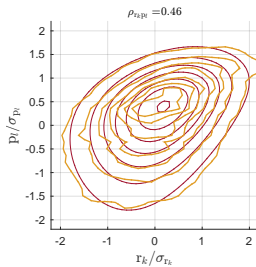
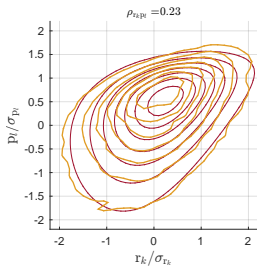
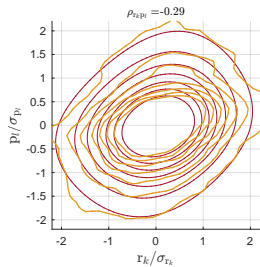
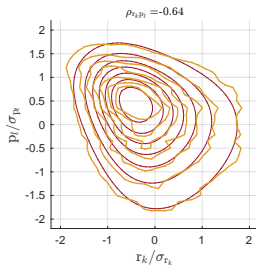
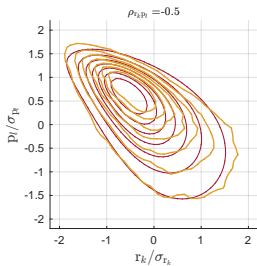
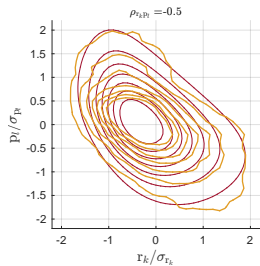
		Response $r_i^m$				
		0	1	2	3	4
Pressure $p_k^n$	0		$\mu_r$	$\sigma_r$	$\gamma_{3,r}$	$\gamma_{e,r}$
	1	$\mu_p$	$\rho_{rp}$			
	2	$\sigma_p$				
	3	$\gamma_{3,p}$				
	4	$\gamma_{e,p}$				
					$E[r_i^m p_k^n]$	

Gaussian assumption

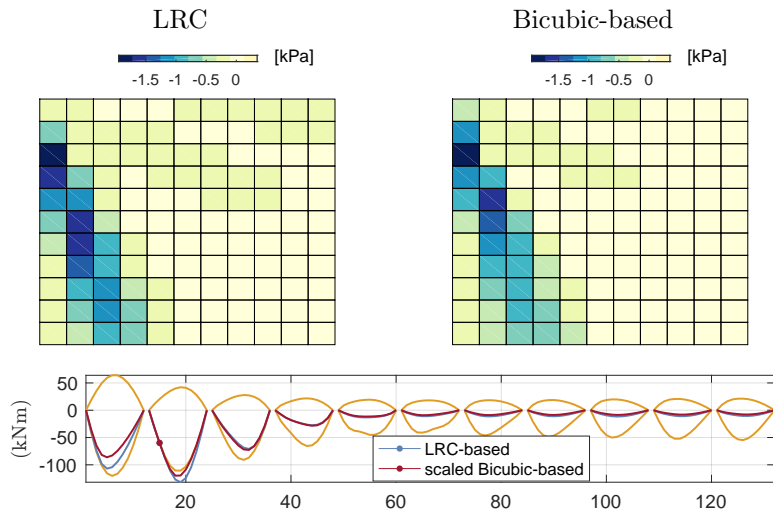
Bicubic Model

# Equivalent Static Wind Load

▷ Bicubic Model (7-parameter)



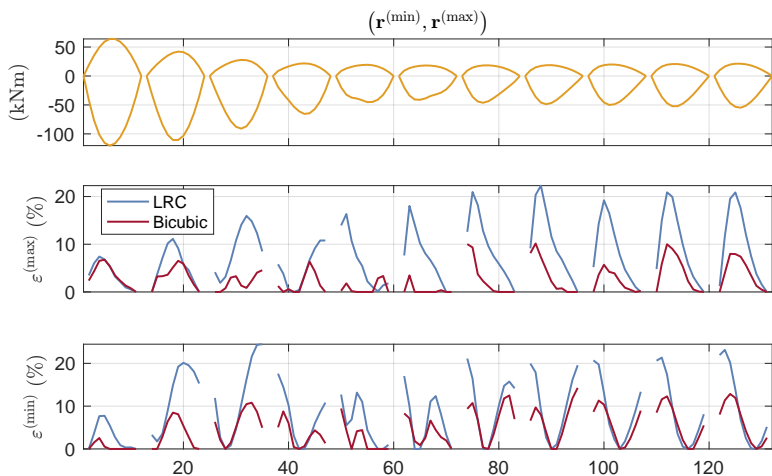
# Equivalent Static Wind Load: Comparison



- LRC: Severe 20% over-estimation of the envelope
- Bicubic-based ESWL: Slight 5% over-estimation of the envelope

# Envelope Reconstruction

▷ Reconstruction of the 86%-quantiles extremes envelope for a reference period of 1 hour.

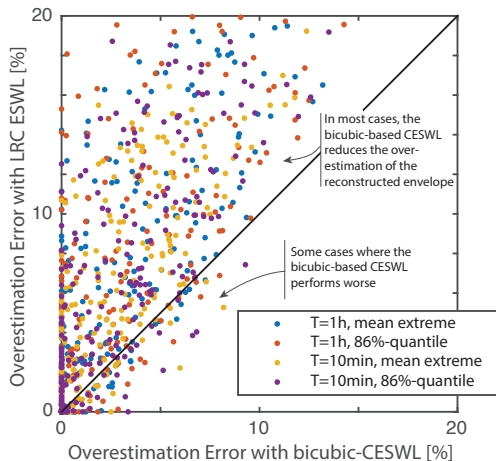


Overestimations up to 25% with the LRC method and up to 15% for the bicubic model



# Envelope Reconstruction

▷ General comparison between LRC ESWL and Bicubic-based ESWL

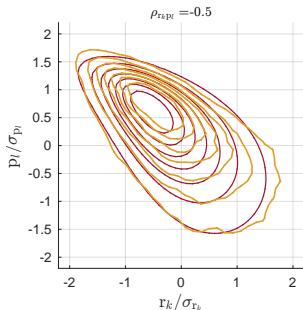


bicubic-based CESWLs generally perform better, but not always.

# Perspectives & Conclusions

## Proposition of a Non-Gaussian version of the LRC

- ▷ bi-cubic model
- ▷ regularly **extends** the LRC for non Gaussian pressure field/responses
- ▷ 7 degrees-of-freedom: fairly good match the non Gaussian joint PDF



# Thank you ...

Vincent Denoël, Université de Liège  
Structural & Stochastic Dynamics  
[www.ssd.ulg.ac.be](http://www.ssd.ulg.ac.be)

## Read more about this topic:

- ▶ Blaise N., Andrienne T., Denoël V. (2017) *Assessment of extreme value overestimations with equivalent static wind loads*. Journal of Wind Engineering and Industrial Aerodynamics 168, 123-133.
- ▶ Blaise N., Canor T., Denoël V. (2016). *Reconstruction of the envelope of non-Gaussian structural responses with principal static wind loads*. Journal of Wind Engineering and Industrial Aerodynamics 149, 59-76.
- ▶ Blaise N., Denoël V. (2013). *Principal static wind loads*. Journal of Wind Engineering and Industrial Aerodynamics 113, 29-39.
- ▶ Kasperski M., (1992). *Extreme wind load distributions for linear and nonlinear design*. Engineering Structures 14, 27-34
- ▶ Holmes J.D., (1988). *Distribution of peak wind loads on a low-rise building*. Journal Of Wind Engineering and Industrial Aerodynamics 29, 59-67

Available @ [www.orbi.ulg.ac.be](http://www.orbi.ulg.ac.be)