

Design and Modelization of a convex grating for the hyperspectral imager Chandrayaan 2: spectral optimization based on free form profile

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1 Introduction

- Goal
- Chandrayaan 2 hyperspectral instrument

2 Design and modelization of a convex grating for Chandrayaan 2

- Choice and optimization of the hyperspectral imager configuration
- Design and modeling of a convex grating for Chandrayaan 2 in the range of $0.7\text{-}5\ \mu\text{m}$
- Realistic profile impact on the diffraction efficiency and the polarization sensitivity
- Diffraction efficiency and Polarization sensitivity depending on incidence angle
- Characterization of the grating

3 Conclusions and Perspectives

Goal

The aim of our work is to distribute the grating diffraction efficiency over a spectral range that goes from 0.7 to 5 μm using free-form grating based on the multi-level profile to meet the diffraction efficiency requirements.



FIGURE 1: *Multi-level grating*

After manufacturing by diamond turning of the grating by Advanced Mechanical and Optical Systems (AMOS), HOLOLAB proceeds to its characterization to check performances.

Chandrayaan 2 hyperspectral instrument

Chandrayaan 2 is an hyperspectral instrument for observing the moon in the infrared. It includes a telescope and a grating spectrometer. AMOS is the project leader and HOLOLAB deals with the design, modeling and optical characterization of the grating (profiles).

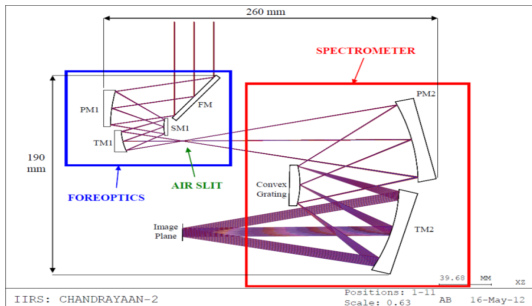


FIGURE 2: *chandrayaan 2 hyperspectral Instrument (AMOS)*

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The choice was focused on the Offner configuration. The optimization is done using Zemax software (AMOS). This configuration offers many advantages including :

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- Diffraction efficiency requirements

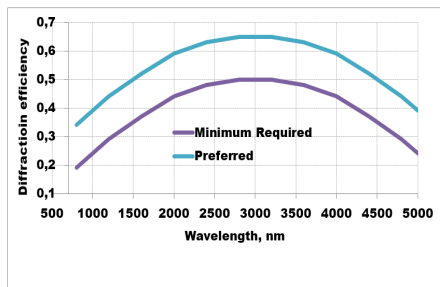


FIGURE 3: Reference curves of the diffraction efficiency

Simulation tools

- 1 Scalar theory

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- 2 Rigorous theory

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Scalar theory

The diffraction efficiency of a grating in reflection is given by the following formula according to this theory

$$\eta_{dif} = \text{sinc}^2 \left(\frac{2h}{\lambda} - k \right) \quad (1)$$

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k : diffraction order and h is the depth of the grooves directly related to the blaze wavelength :

$$\lambda_b = \frac{2h}{k} \quad (2)$$

By combining the two equations for +1 order, we obtain :

$$\eta_{dif} = \text{sinc}^2 \left(\frac{\lambda_b}{\lambda} - 1 \right) \quad (3)$$

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Validity of this theory

Scalar theory is valid in the following case :

$$\frac{\Lambda}{\lambda} \geq 10 \quad (4)$$

Where Λ is the grating period

Rigorous theory : PCgrate software

This theory uses the integral method for solving Maxwell equations. It gives information about polarization sensitivity.

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profile construction

The following profile is for a blaze wavelength of 3000 nm. Note that the axes are not at the same scale.

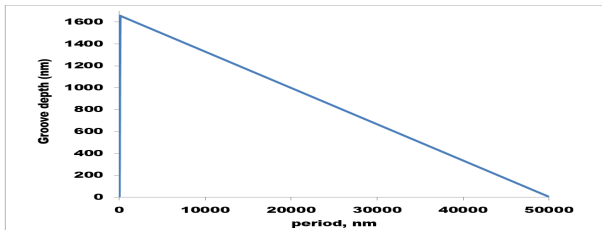


FIGURE 4: *ideal Profile for a central wavelength of 3000 nm*

The diffraction efficiency calculated at blaze wavelength of 3000 nm
By scalar theory

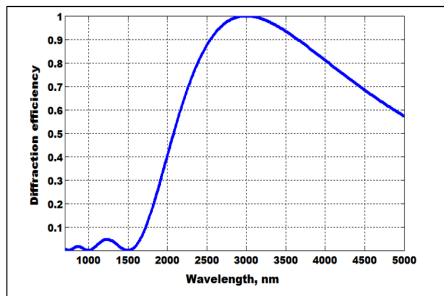


FIGURE 5: *Diffraction efficiency of a grating at a blaze wavelength of 3000 nm given by the scalar theory*

Design and modeling of a convex grating for Chandrayaan 2

The diffraction efficiency calculated at blaze wavelength of 3000 nm

By scalar theory

By rigorous theory

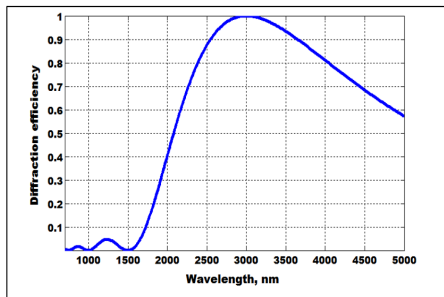


FIGURE 5: Diffraction efficiency of a grating at a blaze wavelength of 3000 nm given by the scalar theory

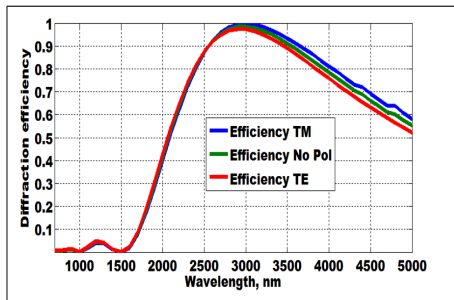


FIGURE 6: Diffraction efficiency of a perfect grating at a blaze wavelength of 3000 nm given by the rigorous theory

Conclusions

- The results of the rigorous theory for a perfect grating confirm those of the scalar theory.

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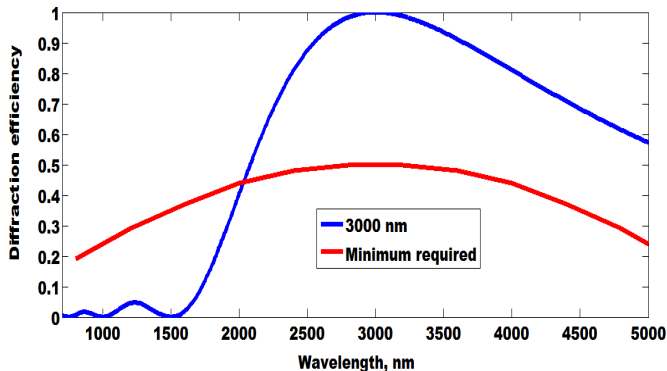
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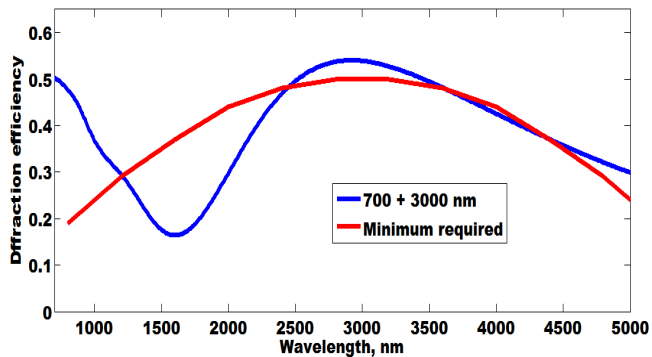
Solution

The multi-blaze method seems most appropriate to solve this problem : I propose a multi-blaze grating with 9 blaze wavelengths which give to the grating a multi-level character. The 9 blaze wavelengths are : 700, 1000, 1400, 1800, 2200, 2500, 3000, 3300 and 4400 nm.

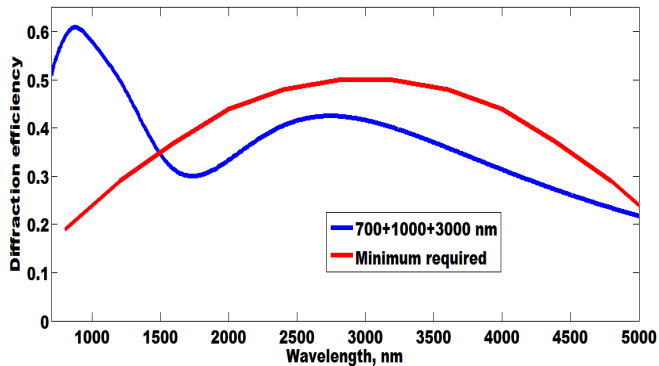
Methodology



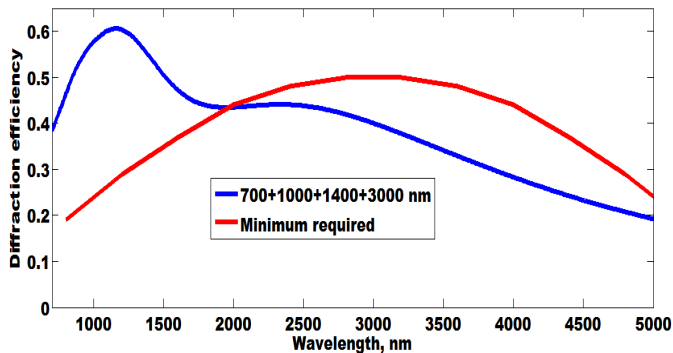
Methodology



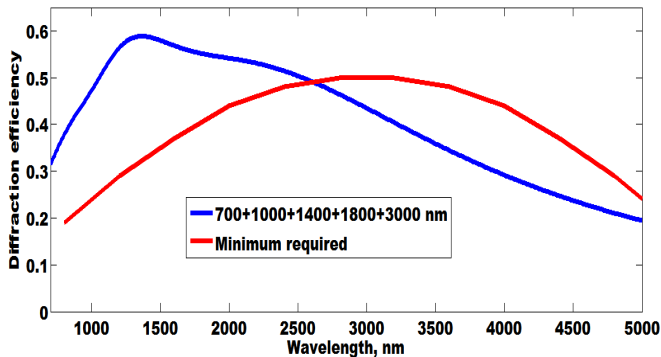
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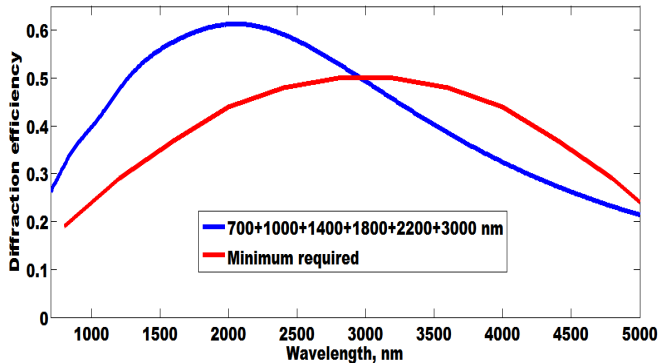
Methodology



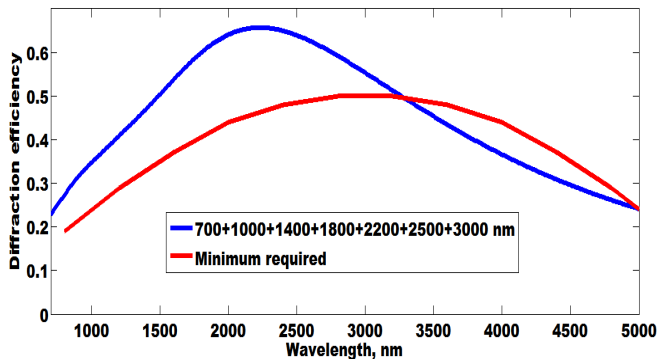
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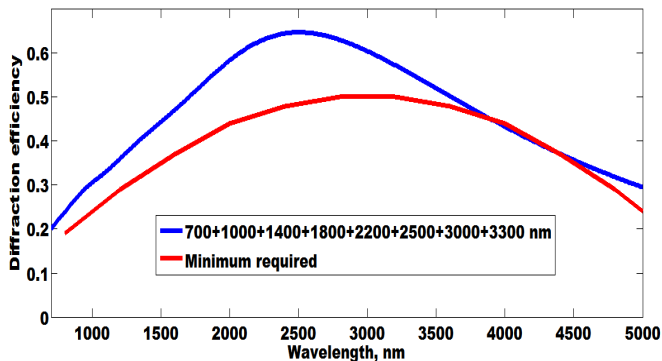
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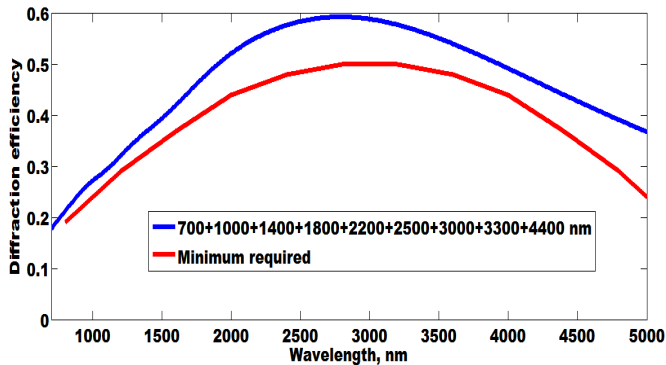
Methodology



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Calculation of the diffraction efficiency of the multi-blaze grating By scalar theory

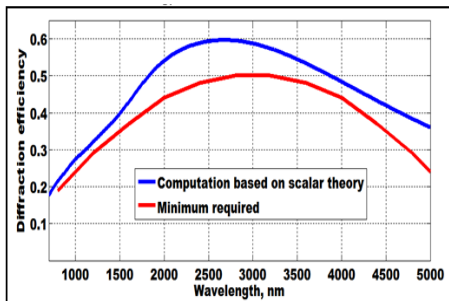


FIGURE 7: Diffraction efficiency of multi-blaze grating by scalar theory

Design and modeling of a convex grating for Chandrayaan 2

Calculation of the diffraction efficiency of the multi-blaze grating

By scalar theory

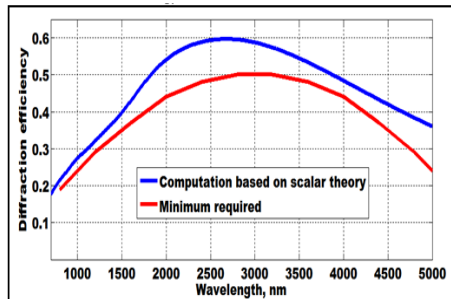


FIGURE 7: Diffraction efficiency of multi-blaze grating by scalar theory

By rigorous theory

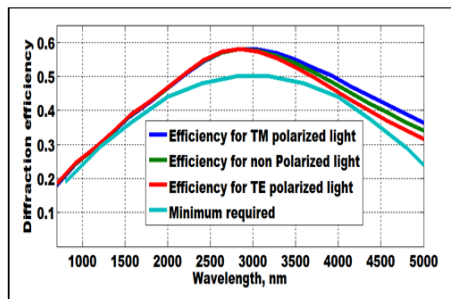


FIGURE 8: Diffraction efficiency of multi-blaze grating by rigorous theory

Conclusions

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- Scalar theory does not take into account polarization effects.

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

Realistic profile model

According to the diamond tool, the realistic profile that we consider is a profile flattened at the top on $5\ \mu\text{m}$, rounded down to the last $3\ \mu\text{m}$ with a radius of curvature of $5\ \mu\text{m}$ (less rounded) and another with a radius of curvature of $10\ \mu\text{m}$ (more rounded) to the last $5\ \mu\text{m}$. The corresponding blaze wavelength is $3000\ \text{nm}$

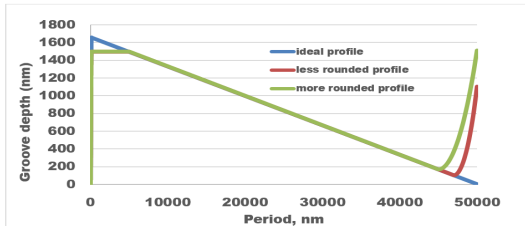


FIGURE 9: *ideal, less and more rounded profiles*

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

Comparison of the diffraction efficiency of the multi-blaze grating with rounded and ideal profiles

ideal profile

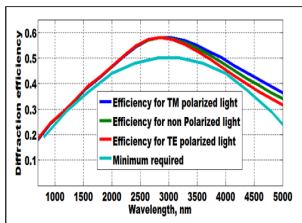


FIGURE 10: *Diffraction efficiency of multi-blaze with ideal profile*

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

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Less rounded profile

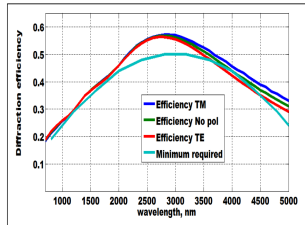
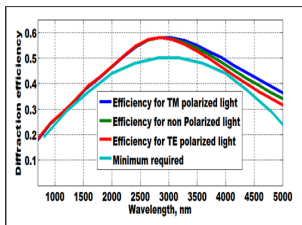


FIGURE 10: *Diffraction efficiency of multi-blaze with ideal profile*

FIGURE 11: *Diffraction efficiency of multi-blaze with less rounded profile*

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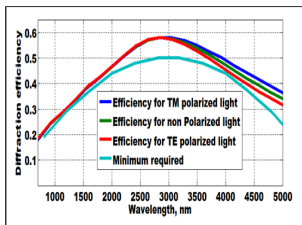


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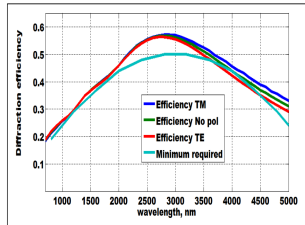


FIGURE 11: Diffraction efficiency of multi-blaze with less rounded profile

More rounded profile

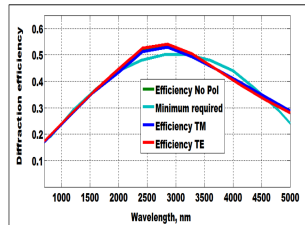


FIGURE 12: Diffraction efficiency of multi-blaze with more rounded profile

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

Conclusion

The diffraction efficiency decreases with the rounded profile. The efficiency decreased by 5 % (absolute) from the ideal profile to the more rounded profile.

Comparison of no polarized efficiencies of the three profiles

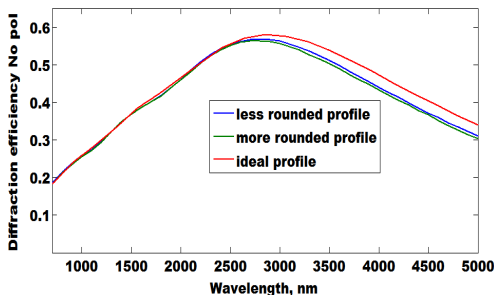


FIGURE 13: No polarized efficiencies of ideal, less and more rounded profile

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

Polarization sensitivity of the multi-blaze grating

The polarization degree of multi-blaze grating is calculated by the following formula :

$$\frac{\eta_{TE} - \eta_{TM}}{\eta_{TE} + \eta_{TM}} \quad (5)$$

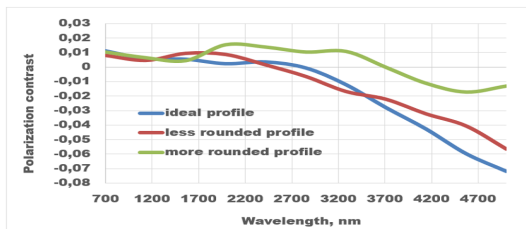


FIGURE 14: Polarization sensitivity of multi-blaze with ideal and rounded profiles

Realistic profile impact on the diffraction efficiency and the polarization sensitivity

Conclusion

The polarization sensitivity decreases with the rounded profile in the middle infrared where the sensitivity is too high. It decreased by 6 % from the ideal profile to the more rounded profile especially at the end of the band.

Diffraction efficiency and Polarization sensitivity depending on incidence angle

The simulation is done for a wavelength of 3000 nm

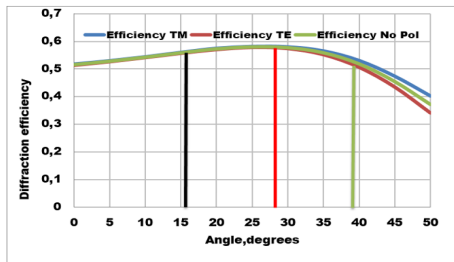


FIGURE 15: Diffraction efficiency as function of incidence angle

Diffraction efficiency and Polarization sensitivity depending on incidence angle

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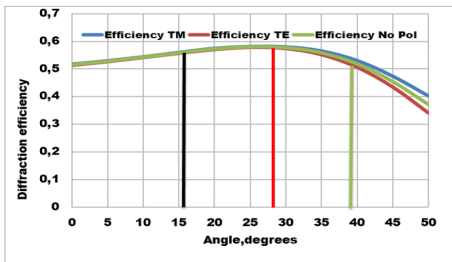


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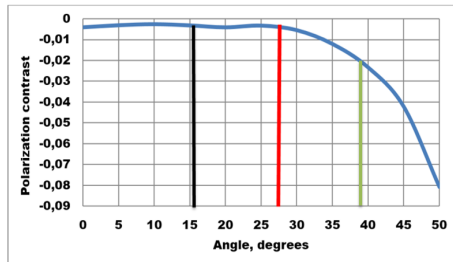


FIGURE 16: Polarization sensitivity as function of incidence angle

Diffraction efficiency and Polarization sensitivity depending on incidence angle

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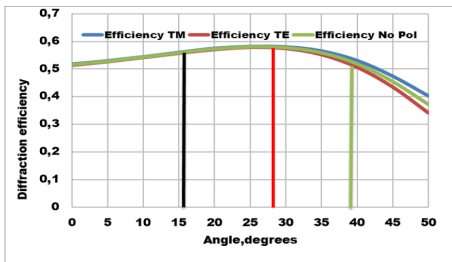


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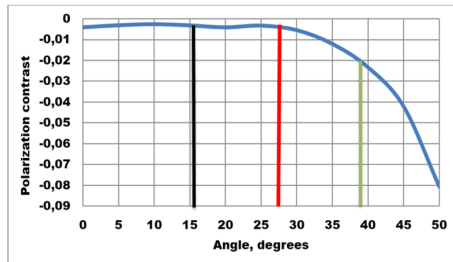


FIGURE 16: Polarization sensitivity as function of incidence angle

Conclusion

The diffraction efficiency varies very little and the polarization sensitivity is low between the 2 working limits.

Characterization of the grating

The characterization will be done using :

Characterization of the grating

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- SuperContinuum IR Source in the spectral range 0.7 to 4 μm

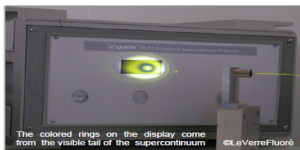


FIGURE 17: IRguide[®] SC-01

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FIGURE 17: IRguide[®] SC-01

- A6700sc Camera FLIR



FIGURE 18: A6700SC Camera

Characterization of the grating

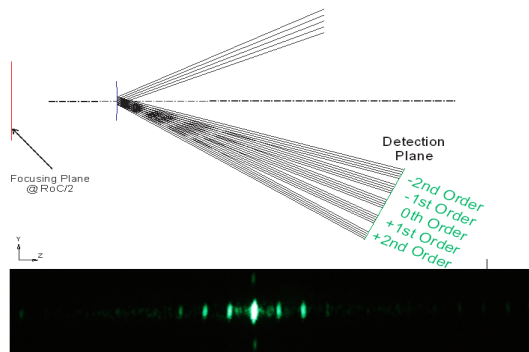


FIGURE 19: *Experimental setup(ESA ITT AO/1-7022)*

Characterization of the grating

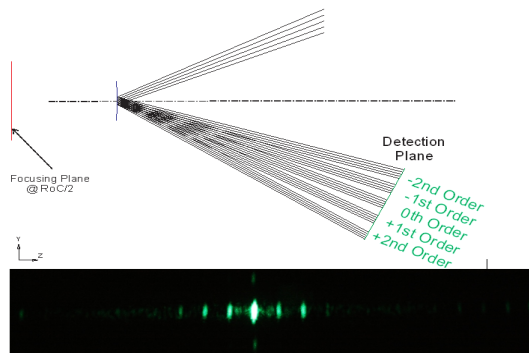


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FIGURE 20: *Free Form Grating*

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In perspective, I am working on a dual angle profile which can be used to optimize a grating in two diffraction orders.

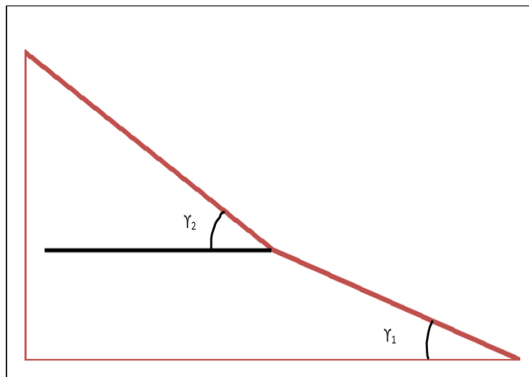


FIGURE 21: *Model of dual angle profile*

Thank you for your attention

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