





Coopération scientifique Québec / Wallonie-Bruxelles

SURFACE CHARACTERIZATION METHODS FOR QUALITY CONTROL OF REPAIRS









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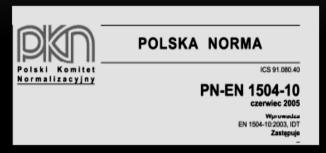
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REPAIR EFFICIENCY EVALUATION



bond strength



bond quality

... should be evaluated







FACTORS AFFECTING BOND BETWEEN CONCRETE SUBSTRATE AND REPAIR MATERIAL

Factors	Importance		
	1	2	3
Substrate	e character	istics	
Substrate properties	X		
Microcracking			Χ
Laitance			X
Roughness	X		
Cleanliness			X
Overlay characteri	stics & applicat	ion technique	
Pre-wetting		X	
Bonding agents	X		
Overlay properties		X	
Placement	X		
Compaction			X
Curing			X
Environmental conditions			
Time		Х	
Early traffic	X		
Fatigue	Х		
Environment	X		







PREPARATION TECHNIQUES (SILFWERBRAND, 2004)

Removal method	Principle behaviour	Depth action?	Advantages	Disadvantages
Sandblasting & shotblasting	Blasting with sand or steel balls	No	No microcracking, no dust	Not selective
Flame-cleaning	Thermal lance	No	Effective against pollutions and painting	The reinforcement may be damaged, smoke and gas development, not selective
Milling (scarifying)	Longitudinal tracks are introduced by rotating metal lamellas	Yes	Good bond if followed by water flushing	Not selective
Pneumatic (jack) hammers, hand-held or boom-mounted	Compressed-air-operated chipping	Yes	Simple use, large ones are effective	Damages reinforcement and concrete surface, poor working environment, not selective
Grinding	Grinding with rotating lamella	No	Removes uneven parts	Dust development, not selective
Explosive blasting	Controlled blasting using small, densely spaced blasting charges	Yes	Effective for large removal volumes	Difficult to limit to solely damaged concrete, not selective
Water-jetting (hydrodemolition)	High pressure water jet from a unit with a movable nozzle	Yes	Effective, selective, does not damage reinforcement or concrete, improved working environment	Water handling, removal in frost degrees, costs for establishment







METHODS OF SURFACE ROUGHNESS CHARACTERIZATION ANALYZED IN THE PROJECT

Development of Specifications and Performance Criteria for Surface Preparation Based on Issues Related to Bond Strength

Research and Development Office Science and Technology Program

American Concrete Institute Foundation Concrete Research Council,

Final Report ST2017-2886-1



- Concrete surface profile (CSP), in accordance with ICRI Guideline No. 310.2R-2013.
- Sand patch test, in accordance with ASTM E965 (similar to EN 13036-1:2010) and EN 1766.
- Mechanical profilometry.
- Laser technique.
- Interferometric profilometry.







CONCRETE SLABS TESTED IN THE PROJECTS

Group A: Grinding (GR), sandblasting (SB), shotblasting (SHB20, SHB35 and SHB45, with treatment times of 20, 35, and 45 seconds, respectively), hand milling (HMIL) and mechanical milling (MMIL); untreated concrete samples (NT) were also tested as a control; **Group B:** Polishing (PL), dry sandblasting (SB-D), jack hammering (JH) and water jetting at 250 MPa pressure (HD);

Group C: Gentle surface preparation methods were used to obtain profiles of similar amplitude and low-level microcracking: brushing (NT), wet sandblasting (SB-W), scarifying (SC) and water jetting at 12 MPa pressure (LC).







VISUAL OBSERVATION (1)

grinding



sandblasting



shotblasting



milling









VISUAL OBSERVATION (2)

CSP1	CSP2	CSP3
2.4. (P-8.2		
	の対象を	
CSP4	CSP5	CSP6
CSP7	CSP8	CSP9
		A 70-200

Surface preparation methods	CSP
Detergent scrubbing	1
Low-pressure water cleaning	1
Acid etching	1–3
Grinding	1–3
Abrasive blasting (sand)	2–5
Steel shotblasting	3–8
Scarifying	4–9
Needle scaling	5–8
Water jetting	6–9
Scabbling	7–9
Flame blasting	8–9
Milling/rotomilling	9







SAND PATCH TEST







ASTM E965 (very similar to EN 13036-1). The surface roughness is characterized using glass or sand particles by the mean texture depth (MTD):

$$MTD = \frac{4V}{\pi D^2} [mm]$$

$$SRI = \frac{V}{D^2} \cdot 1272 \qquad V = 25 \text{ mL}$$

V = volume of granular material [mm³]; D = diameter of circle covered by granular material [mm]





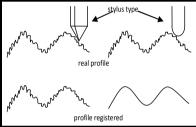


MECHANICAL PROFILOMETER

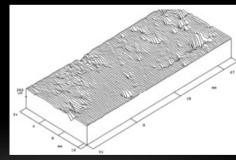
L.Courard, M. Nélis

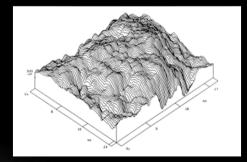
a high-precision extensometer is moved over the entire. surface to obtain a 3D map (with x, y and z coordinates) from which morphological parameters are computed













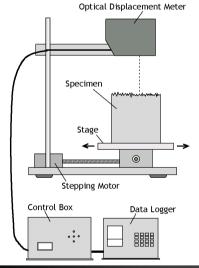




LASER PROFILOMETER

the superficial elevation (distance from the laser beam source to the object) of each point is calculated on the basis of the laser beam transit time.





Treatment	Waviness	Roughness
As-received, no treatment NT	1.48 mm	0.75 mm 0.2 mm
Grinding GR	1.08 mm	112 µm 7.6 mm 27.6 mm
Sandblasting SB	1.22 mm	2.501 mm
Shotblasting 35s SHB35	3.09 mm	3.834 mm 9.2 mm
Hand Milling HMIL	1.46 mm	0.53 mm
Mechanical Milling MMIL	3.85 mm	3.504 mm

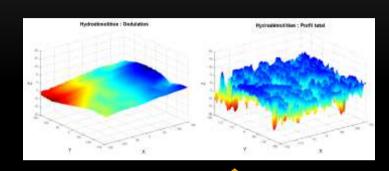




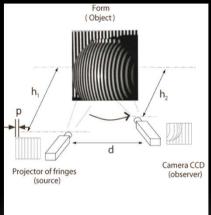


INTERFEROMETRIC PROFILOMETRY

based on observation and analysis of the shadow produced by the superficial roughness of the surface (moiré fringe pattern principle)











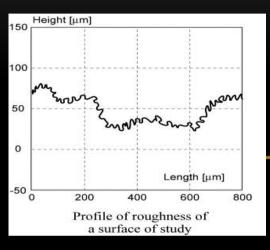




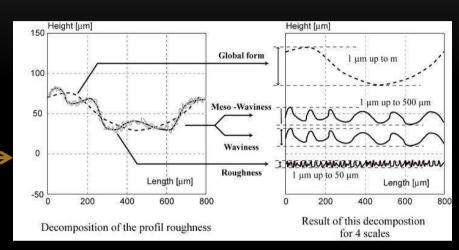




GEOMETRICAL PARAMETERS OF SURFACE STRUCTURE ACC. PN-EN ISO 4287 (1):



profile filtration



Roughness	high frequencies gap between grooves (amplitude) R _m is 5-100 times the depth R _t	Rm roughness: $R_m = (5100) \cdot R_t$
Waviness	mean frequencies amplitude W _m is 100- 1000 times the depth of holes W _t	waviness: W _m = (1001000)·W ₀ Wm



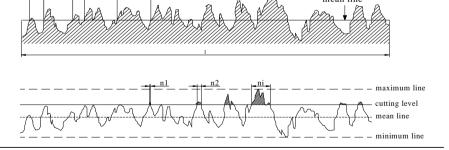




GEOMETRICAL PARAMETERS OF SURFACE STRUCTURE ACC. PN-EN ISO 4287 (2):

1	ym- ool	Parameters	Definition
m	n _x	mean value and line	line whose height (mean value) is determined by minimal sum square deviation of the profile defined as follows: $X = \min \sum y^2(x)$
Х	X _p	max peak height	distance between the highest point of the profile and the mean line
Х	ζ _m	max valley depth	distance between the lowest point of the profile and the mean line
>	X _t	max height	maximum distance between the lowest and the highest point of the profile and it's equal $X_t = max (X_p + X_m)$
	X _a	arithmetic mean deviation	mean departure of the profile from the reference mean line as follows: $X_a = \frac{1}{l} \int_0^l y(x) dx \text{, approximated by } X_a \approx \frac{1}{n} \sum_{i=1}^n y_i $
×	X _q	Root mean square deviation	statistical nature parameter it is defined in the limits of the cut-off length $X_q = \frac{1}{l} \int_0^l y^2(x) dx$

Sy m- bol	Parameters	Definition
Sk	skewness of surface height distribution	a measure of asymmetry of profile deviations about the mean line, as follows: $S_k = \frac{1}{R_q^3} \frac{1}{n} \sum_{i=1}^n Y_i^3$
S _m	mean period of profile roughness	mean value of mean line including consecutively a peak and a valley S_{mi} , as follows: $S_m = \frac{1}{n} \sum_{i=1}^n S_{mi}$
n _p	bearing length	sum of partial lengths ni corresponding to the profile cut by a line parallel to the mean one for a given cutting level
tp	bearing length ratio	ratio between bearing length and cut-off length, given as a percentage (%): tp = np/l.

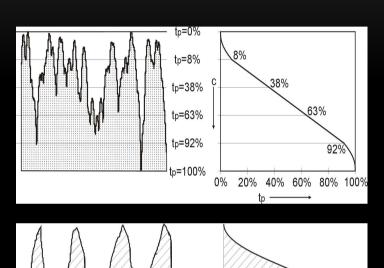


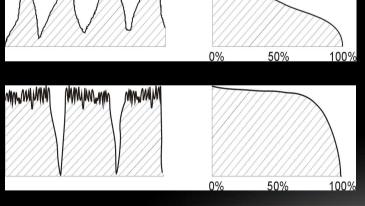






GEOMETRICAL PARAMETERS OF SURFACE STRUCTURE ACC. PN-EN ISO 4287 (3):





Bearing curve

(Abbot's curve)

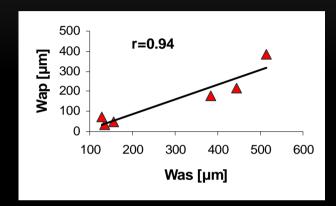
Sym -bol	Parameters	Definition
C_R	relative height of the peaks	gives an idea of significance of the volume of very high peaks above the reference line
C _F	depth of the profile	excluding high peaks and deep holes gives information on surface flatness; a lower value of C _F means an important surface flatness
C _L	relative depth of the holes	gives an idea of the significance of the volume of voids under the reference line

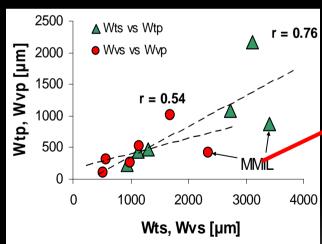


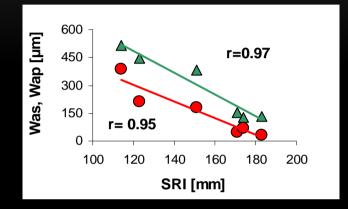


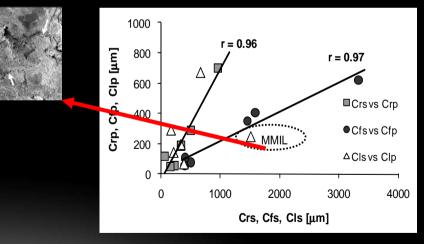


MECHANICAL (P) VS. LASER (S) PROFILOMETRY (1)







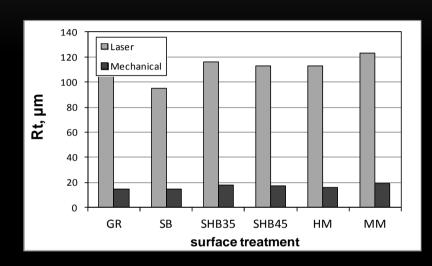


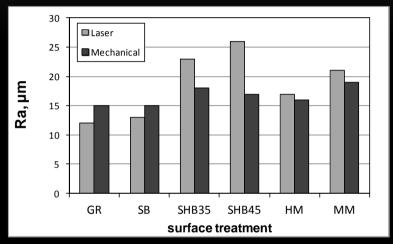






MECHANICAL (P) VS. LASER (S) PROFILOMETRY (2)





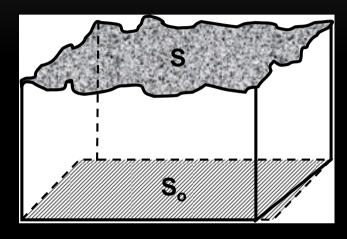
surface treatment technique does not have much influence on microroughness (high-frequency waves). The waviness parameters actually need to be determined in order to assess surface roughness prior to repair





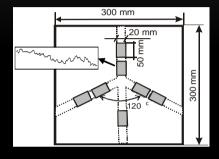


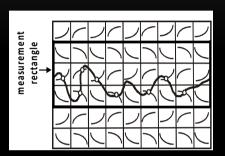
SURFACE ROUGHNESS CHARACTERIZATION WITH THE MICROSCOPIC OBSERVATION METHOD

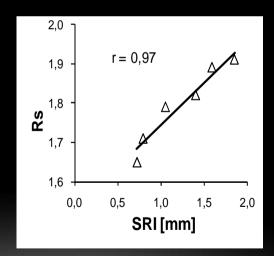


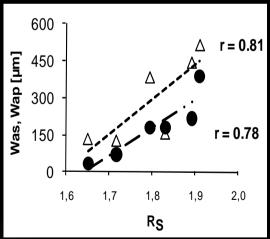


surface roughness is related to the energy being dissipated during material decohesion











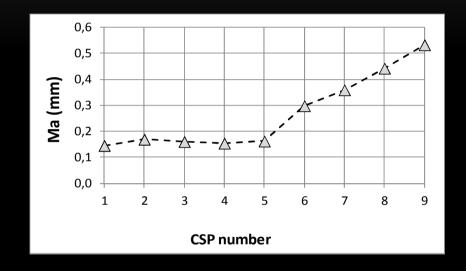




INTERFEROMETRY VS CSP







The actual CSP plates are rather narrow with respect to the spectrum of CSPs obtained with actual surface preparation techniques.







SUMMARY

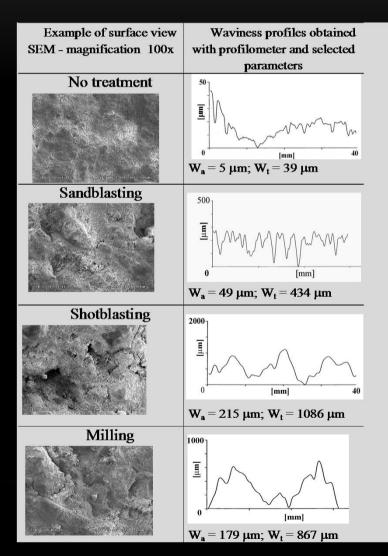
- ☐ Characterization of surface roughness is an important aspect in assessing a concrete substrate prior to repair. Various techniques have recently been available for CSP characterization.
- ☐ The waviness parameters actually need to be determined in order to assess surface roughness prior to repair.
- Among the techniques available today, the best suited method for field assessment appears to be the CSP developed by ICRI.

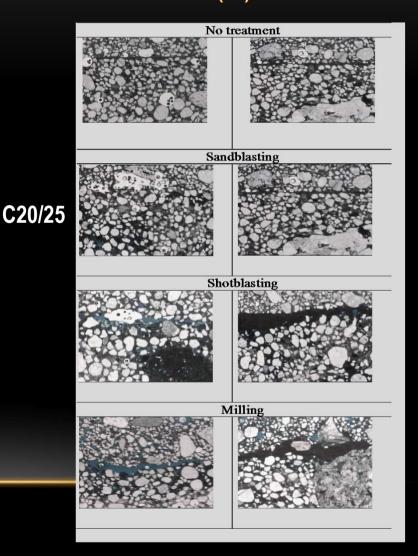






ADHESION VS. SUBSTRATE QUALITY (2)





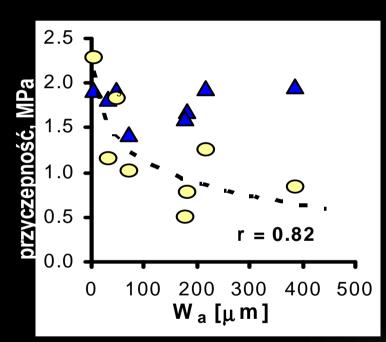


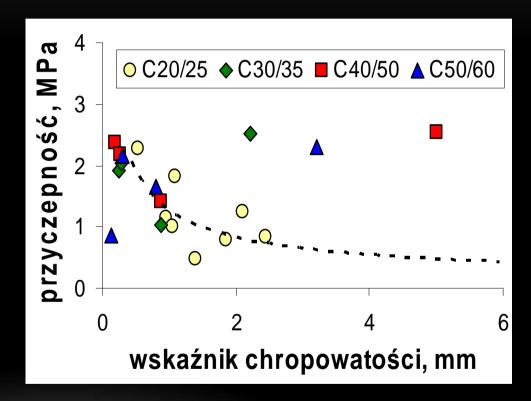




ADHESION VS. SUBSTRATE QUALITY (2)





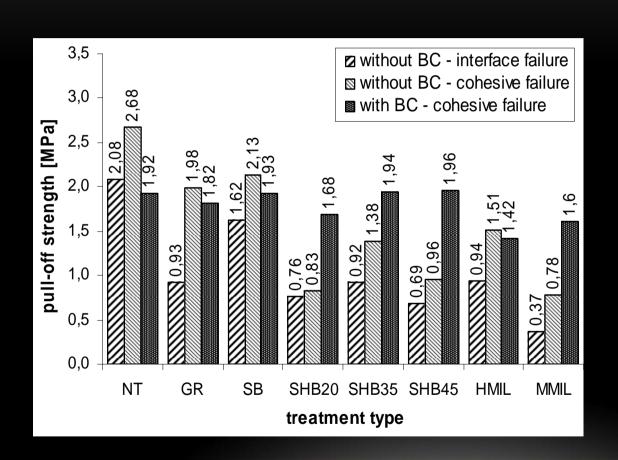


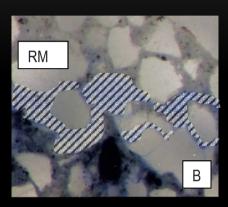






ADHESION VS. SUBSTRATE QUALITY (3)





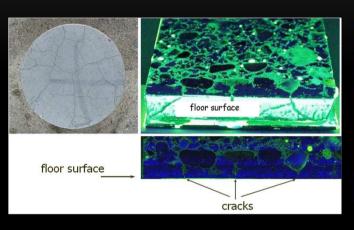




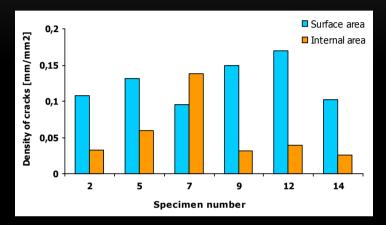


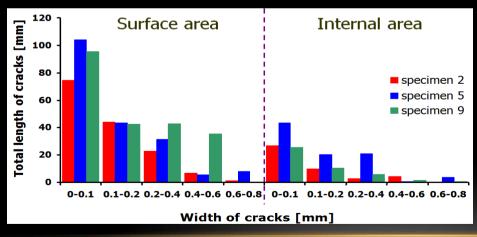


MICROCRACKING EVALUATION (1)









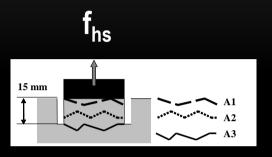
M.Glinicki, A.Litorowicz, 2005

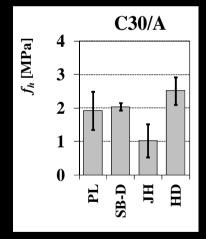


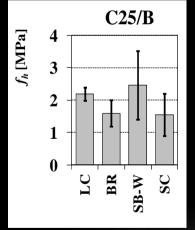


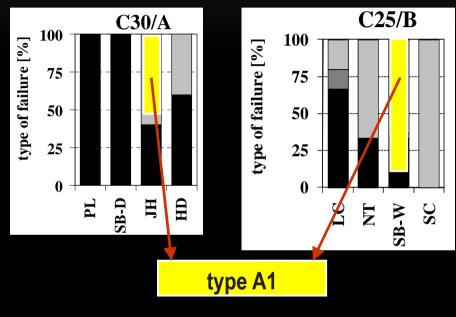


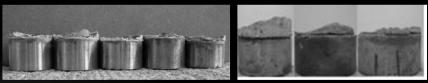
MICROCRACKING EVALUATION (1)









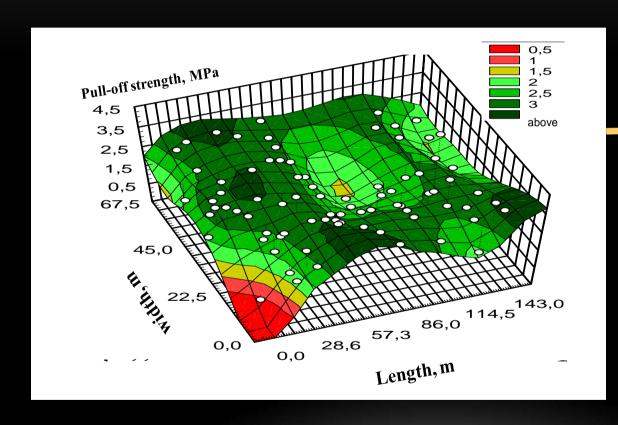








PULL OFF IS THE MOST COMMON TEST



→ NDT!

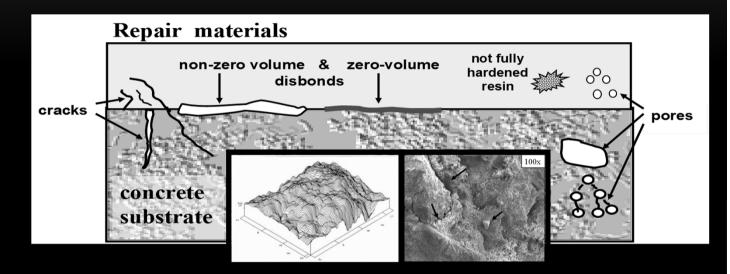
Impact-echo Ultrasonic GPR







REPAIR SYSTEM AS AN OBJECT OF NDT TESTING



DEFECT TYPES

- Adhesion type (at the interface zone of RM-CS system): non-zero volume debonding (delamination), zero-volume debonding, weak adhesion areas
- Cohesion type (in repair material or/and concrete substrate): porosity, cracks, honeycombing, unhardened resin (PC)

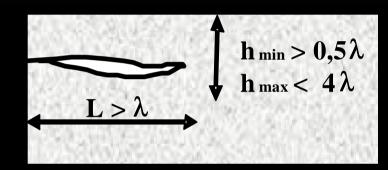






SELECTION OF NDT METHOD

- Defect size & depth
- Repair material thickness
- Repair material type (R coeff.)
- Substrate quality



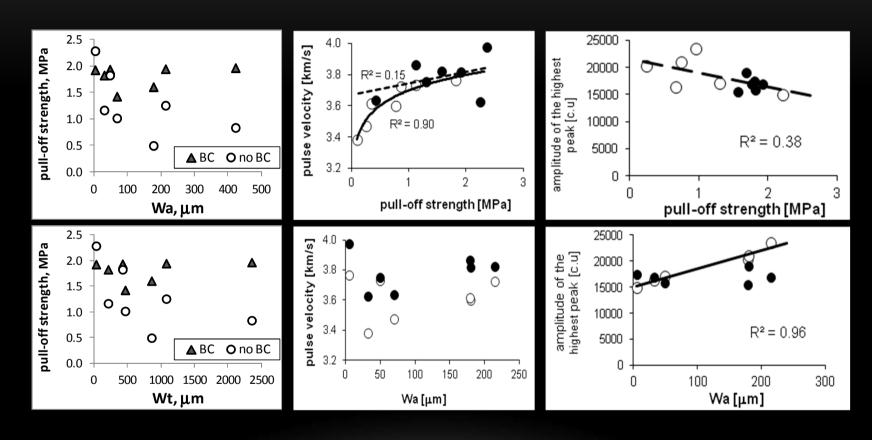
$$R = \frac{A_r}{A_i} = \frac{Z_2 - Z_1}{Z_2 + Z_1}$$







RESULTS









CONCRETE SUBSTRATE QUALITY (2)

Group A

Group B

Concrete

C30/37, C40/50, C50/60

Surface preparation

no treatment **NT**wet sandblasing **SB-W**scaryfication **SC**water jetting **LC**

polishing **PL**dry sandblasting **SB-D**jack hammering **JH**hydrodemolition **HD**

SRI [mm]

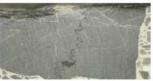


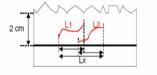




Total length of microcracks [mm]







Bond strength (pull-off) [MPa]



acc. EN 1542

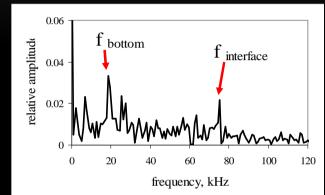




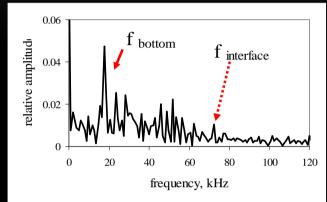


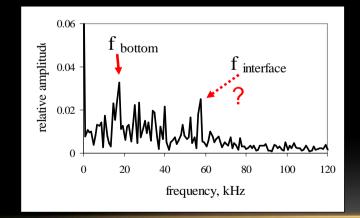
EFFECT OF CONCRETE SUBSTRATE PREPARATION (LAB)

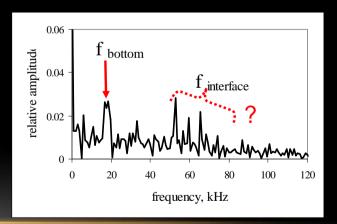




sandblasting







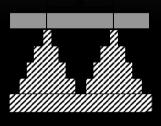




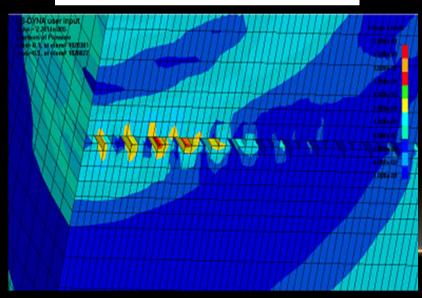


EFFECT OF CONCRETE SUBSTRATE PREPARATION (FEM)

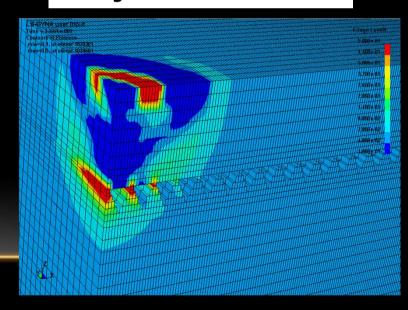




Sandblasting



Hydrodemolition



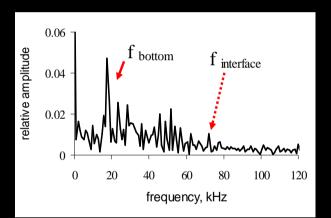




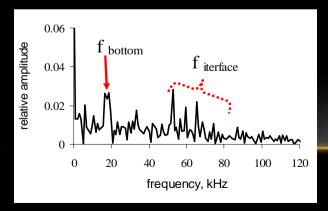


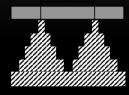
LAB vs. FEM

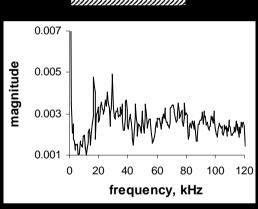
SB:

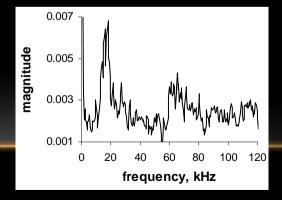


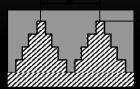
HD:

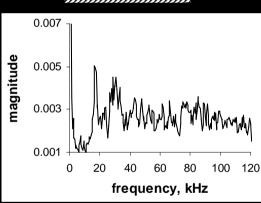


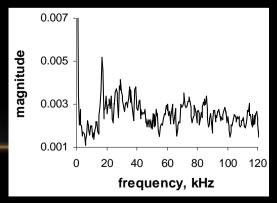


















SUMMARY

- For the both IE and ultrasonic methods, the roughness and microcracking of the concrete substrate do not affect significantly the P-wave propagation through the repair system if the bond quality is sufficient
 - → absence of large voids at the interface







SUMMARY

 Parameters describing roughness and microcracking of concrete substrate can be considered as important variables for improvement of reliability of the bond strength evaluation, using more advanced signal analysis of stress waves (e.g. wavelet approach)







CONCRETE

very good construction material





4th successful







Repair of concrete Never ending story







ACKOWLEDGMENTS

- Concrete Research Council de l'American Concrete Institute (ACI)
- Conseil de Recherche en Sciences Naturelles et en Génie du Canada (CRSNG)
- Fonds de Recherche Québécois sur la Nature et les Technologies (FRQNT)
- U.S. Bureau of Reclamation (USBR)
- Chaire CRSNG sur la Réparation durable et l'entretien optimisé des infrastructures en béton à l'Université Laval (BASF, Euclid, Holcim, Hydro-Québec, Kerneos, King Packaged Materials, Lafarge, Ministère des Transports de Québec, Ville de Montréal, Ville de Québec, W.R. Grace & Co.)
- Programmes de coopération scientifiques des gouvernements polonais, québécois et de Wallonie-Bruxelles







DZIĘKUJĘ! MERCI!











- •January 4, 1826 the Preparatory School for the Institute of Technology,
- •June 8, 1898 Tsar Nikolaus II Institute of Technology,
- •November 15, 1915 Warsaw University of Technology (with Polish as the language of instruction).

