



SECURE WITH STEEL ArcelorMittal, Esch-sur-Alzette Annual meeting - October 27, 2016

New features in SAFIR[®] 2016 Jean-Marc Franssen Thomas Gernay

- 1. Updated GiD-SAFIR interface
- 2. New SAFIR executable release
- 3. New DIAMOND release
- 4. Distribution and evolution policy
- 5. References

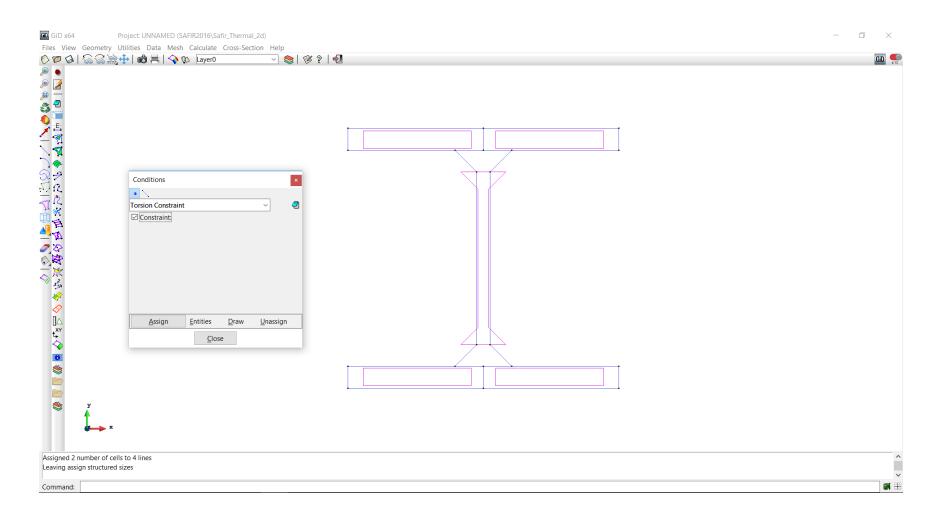
1. GiD

The problem types for creating SAFIR input files have been updated. They have been checked with **version 12 of GiD**.

- Some bugs have been fixed, namely:
 - Modification of the name of the SAFIR executable launched by GiD: the name of the file (to be included in the folder specified in the environment variable defined by the user) should now be "safir.exe" (see sections 4.2 and 4.3 in "SAFIR_installation_guide.pdf");
 - Correction of a bug with Structural 3D cases that include beam elements and shell elements.
- New features have been added, namely:
 - Possibility to fix one node during the torsional analysis ;
 - Possibility to reduce the torsional stiffness by a chosen factor ;
 - Possibility to define tetrahedral elements in Structural 3D cases.

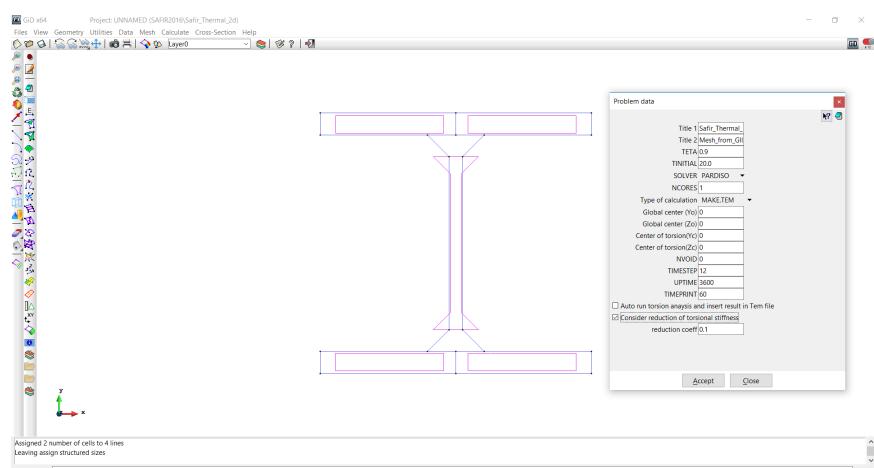
1. GiD

Possibility to fix one node during the torsional analysis



1. GiD

Possibility to reduce the torsional stiffness by a chosen factor (take into account temperature)



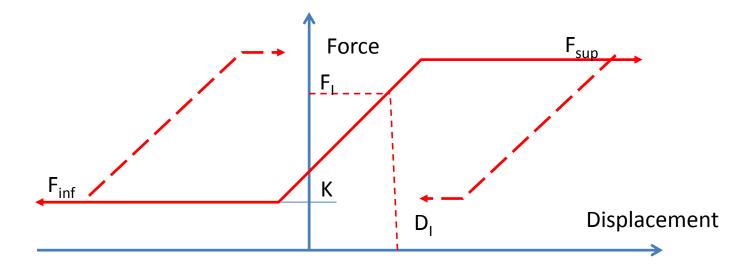
New developments in:

- Capabilities for thermal analysis
- Capabilities for mechanical analysis
- Finite elements
- Material laws
- Solver
- Output files

- Capabilities for thermal analysis
 - New method to heat structural beam finite elements by a localized fire, see
 LOCAFI in the Users manual thermal.

- Capabilities for mechanical analysis:
 - Trapezoidal distributed loads on beams, in local (for wind loads) or in global (for gravity loads) system of coordinates, see TRAPLOCBM and subsequent commands
 - Pressure from water table, following the large displacements of the structure, see NHYDROST and WATERTABLE.
 - Possibility to print the strains that exceed a certain value in the bars of shell finite elements, see PRNSTRAIN.
 - Possibility to specify a maximum value admitted for the displacements, see MAX_DISPL.

- Finite elements:
 - New type of finite element SPRING to link the structure to the foundation, with elasto-plastic behaviour. Allows a more precise representation of the pressure from the ground than a constant pressure.



Input parameters are:

NSPR: Number of the element.

- NNODE: Node where this element is attached.
- CX: Cos of the angle between X axis and this element
- CY: Cos of the angle between Y axis and this element
- CZ: Cos of the angle between Z axis and this element

- F_s Superior limit of the load.
- F_{inf} Inferior limit of the load.
- K Stiffness of the element (elastic loading/unloading)
- A Area of influence (all forces are multiplied by A)
- D_i Displacement in the configuration of reference (t = 0).
- F_i Force in the configuration of reference (t = 0).

• Finite elements: example with springs

2D model with beam F.E. and spring F.E.

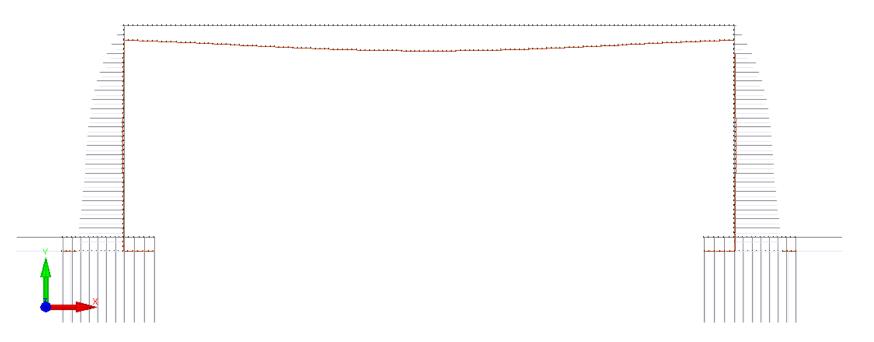


- No restrain
- Trapezoidal loads on the walls replaced by spring F.E.

• Finite elements: example with springs

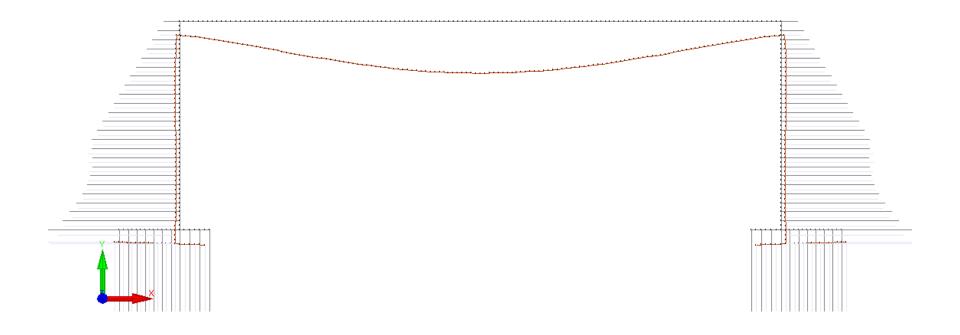
Deformed shape and soil pressures at t = 60 s

Note: Diamond can plot the loads F or the pressure F/A in the spring elements



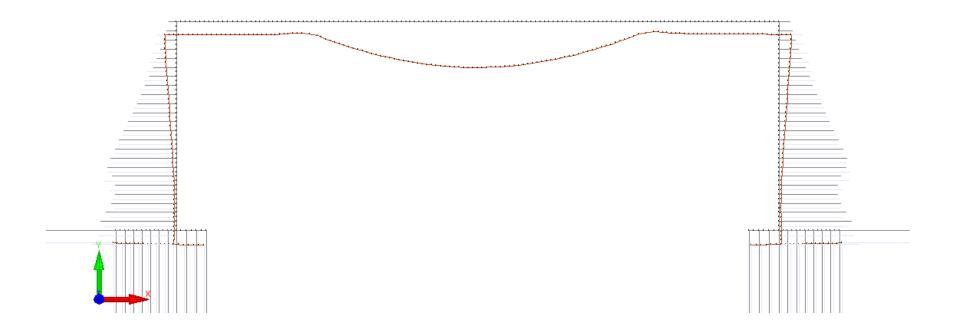
• Finite elements: example with springs

Deformed shape and soil pressures at t = 3720 s (just before plastic hinges appear)



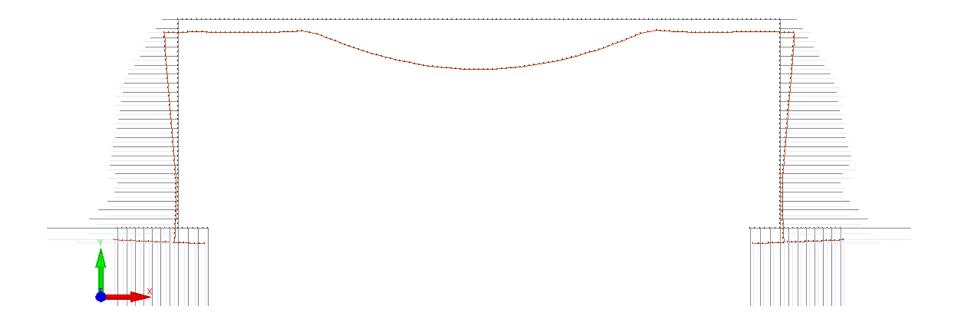
• Finite elements: example with springs

Deformed shape and soil pressures at t = 3800 s (just after plastic hinges appear)



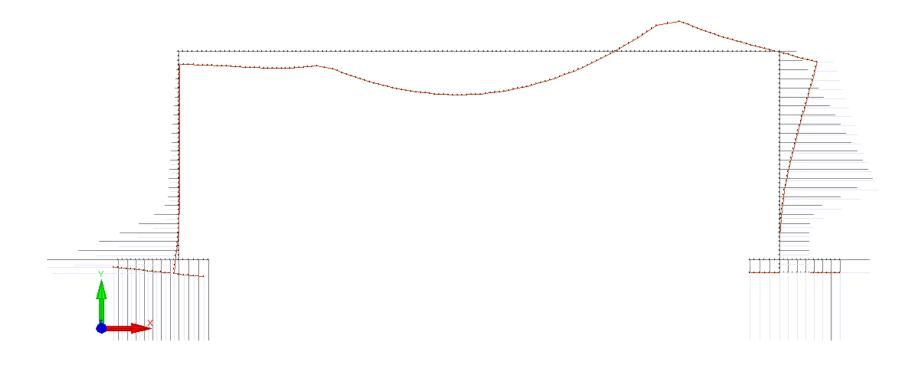
• Finite elements: example with springs

Deformed shape and soil pressures at $t = 5 \ 135 \ s$ (just before failure)



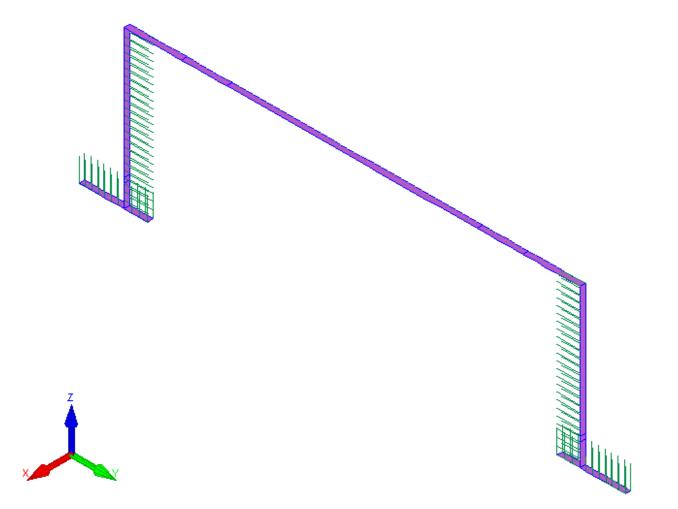
• Finite elements: example with springs

Deformed shape and soil pressures after failure

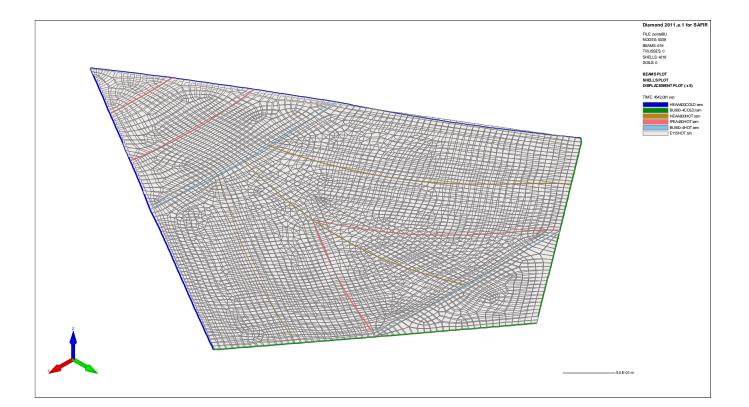


• Finite elements: example with springs

3D model



- Finite elements:
 - Reinforcing bar layers oriented with respect to the global system of coordinates in shell finite elements (very useful in unstructured meshes).



Japan Tobacco Intl, Geneva Model: Ingeni (courtesy Lorenzo Lelli)

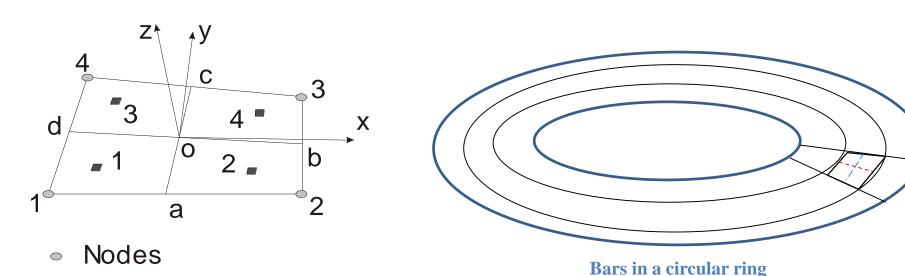
• Finite elements: reinforcing bars in shell

For each bar layer, there are 2 methods to give the orientation of the bars in the plane of the element.

<u>Method 1</u>: with respect to the <u>local</u> system of coordinates of each element.

- 1 card.
- "ANGLE"

- angle Angle in degrees between the local x axis and the layer of rebars, see Figure in which the bars of the layer are represented by doted lines. This angle cannot be smaller than -180° .



Points of integration

Method 1

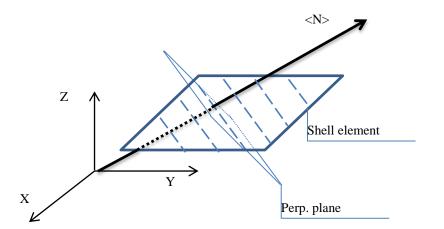
• Finite elements: reinforcing bars in shell

<u>Method 2</u>: with respect to the <u>global</u> system of coordinates of the structure. 1 card.

- "NORMAL"
- N₁
- N₂
- N₃

< $\rm N_1$; $\rm N_2$; $\rm N_3$ > is a vector in the global system of coordinates of the structure. The norm of the vector does not have to be 1.

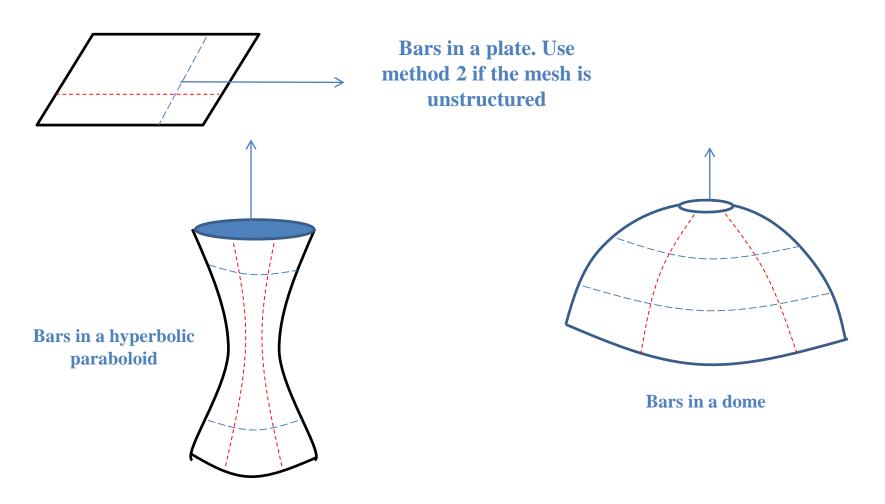
This vector is used to define the position of the bar layers in the shell elements with respect to the global system of coordinates according to the following technique, see Figure.



The bars have the orientation of the line which is the intersection between the shell element and a plane that is perpendicular to the normal.

If the norm of the vector is 0, then the orientation of this bar layer is perpendicular, in each element, to the previous bar layer (not possible for bar layer 1).

• Finite elements: reinforcing bars in shell



ACKNOWLEDGEMENT DEVELOPMENT OF THE SECOND METHOD HAS BEEN SUPPORTED BY « HOLMES FIRE »

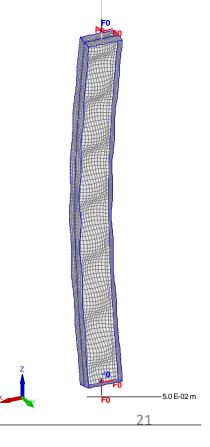
- Material laws:
 - New type of material « STEELSL » to take local buckling into account in beam finite elements.

Steel sections made of slender plates may deform locally (local buckling)

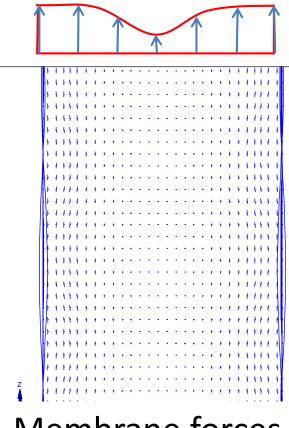




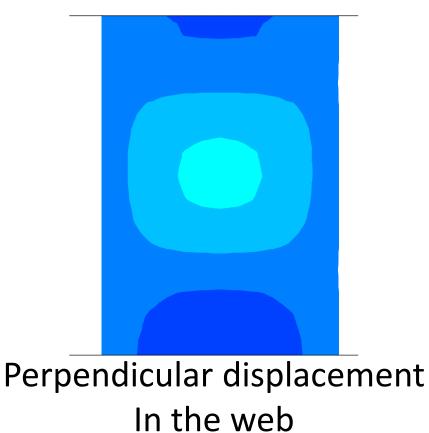
=> They cannot be modelled with beam finite elements



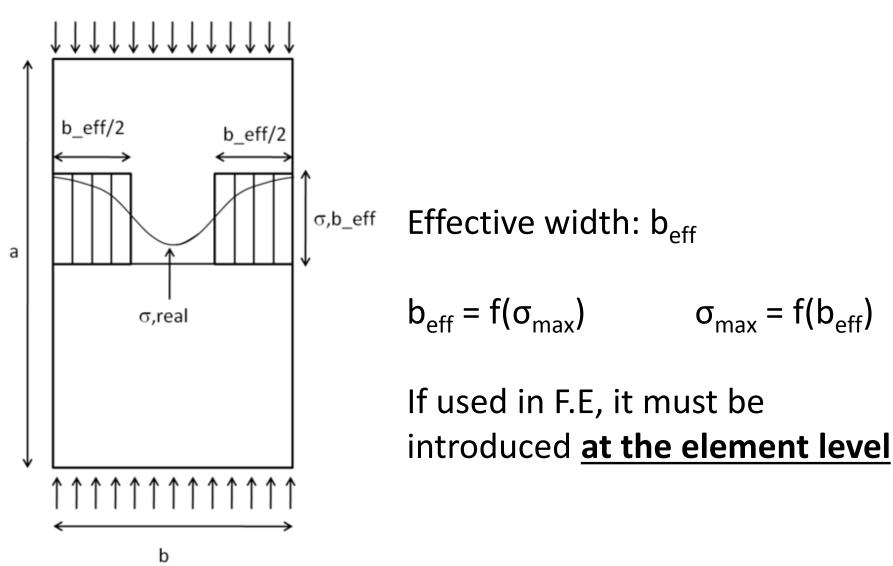
• Material laws: STEELSL



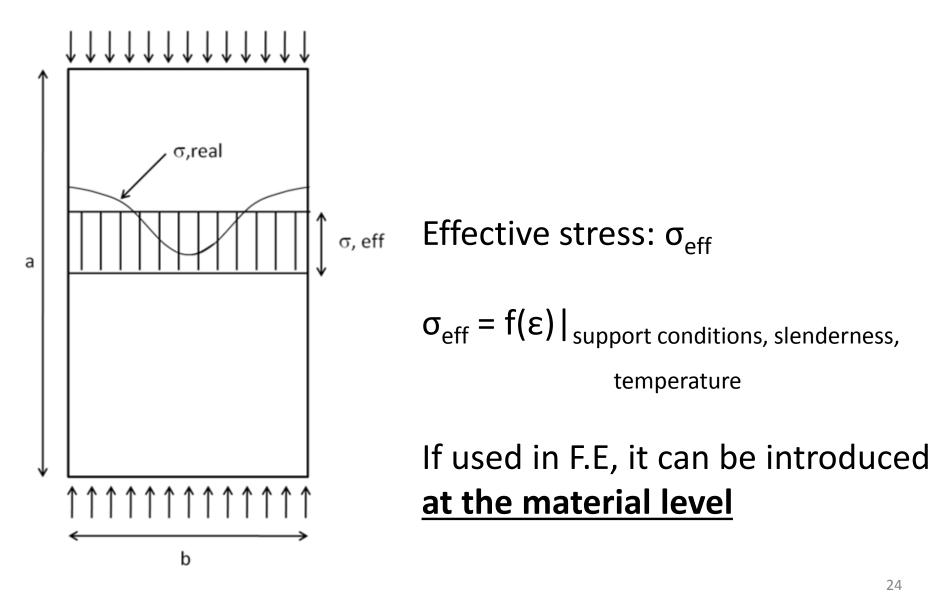
Membrane forces In the web



• Material laws: STEELSL

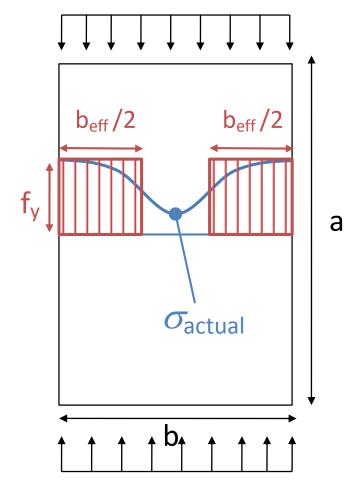


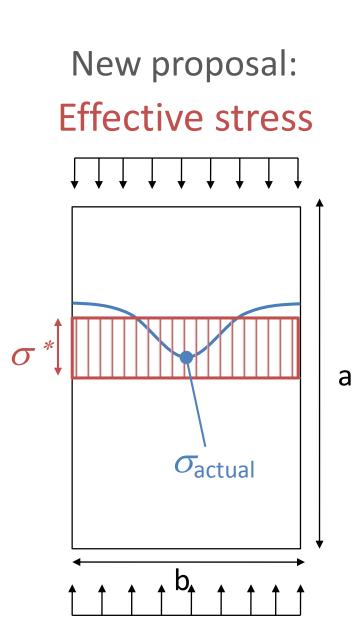
Material laws: STEELSL ۲



• Material laws: STEELSL

Effective width



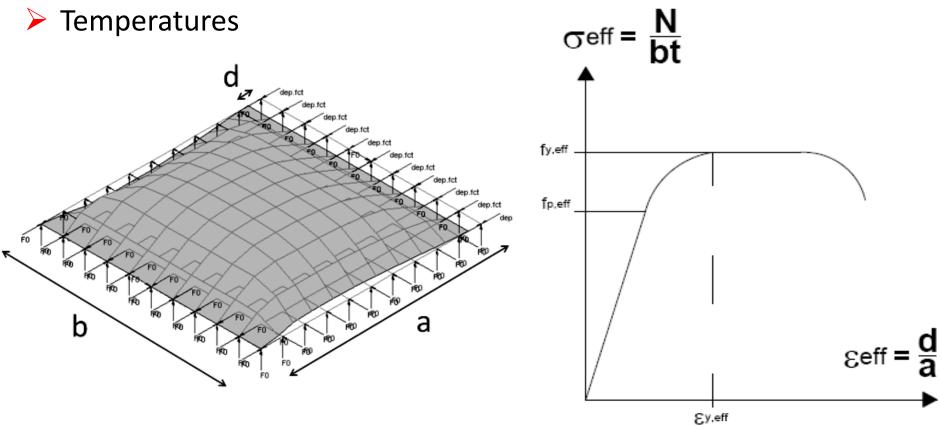


• Material laws: STEELSL

How do we determine $\sigma_{eff} = f(\epsilon)$?

By a series of numerical push-over tests made for different:

- Support conditions
- Plate slendernes

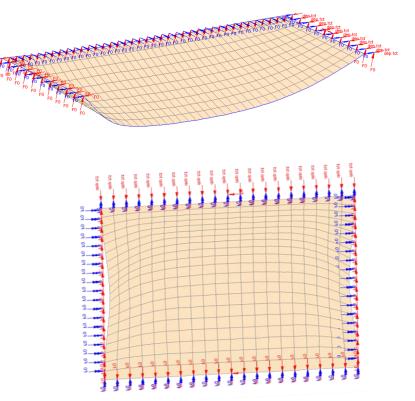


• Material laws: STEELSL

Various support conditions

Flange Simply supported on 3 sides

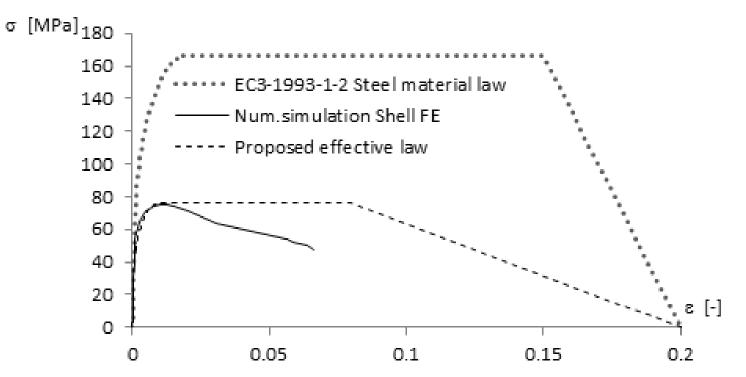
Web Simply supported on 4 sides



• Material laws: STEELSL

The stress-strain relationship is the one of Eurocode 3.

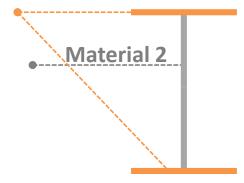
For each combinaison of Temperature – Slenderness - support condition, the values of $f_{p,eff}$ and $f_{y,eff}$ in compression are modified in the material law (E and ϵ_u remain unchanged, as well as all parameters in tension)



• Material laws: STEELSL

The user gives in the input file f_{y} , b/t and the support condition for the web and the flange

Material 1

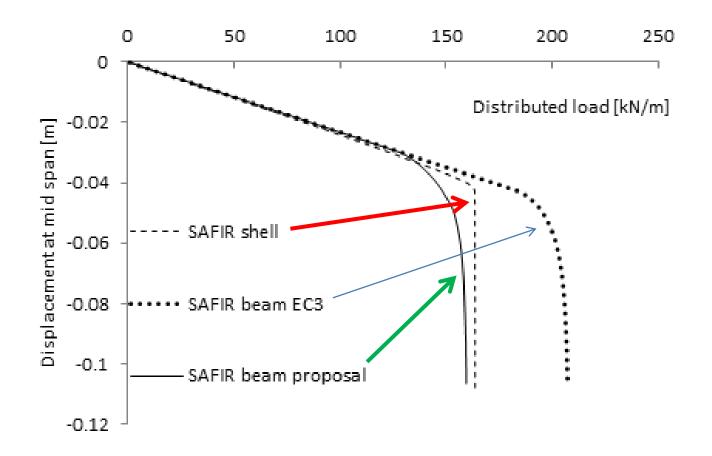


In the members, every point of integration follows its own σ_{eff} - ϵ relationship



• Material laws: STEELSL – Validation against shell FE

Simply suported beam with UDL $T = 20^{\circ}C$ L = 6 metersSection: H = 300x4, B = 150x4



• Material laws: STEELSL – Conclusion

- ✓ The proposed technique is extremely CPU efficient compared to shell F.E.
- It reasonably well accounts for local buckling arising from longitudinal stresses
- ✓ Sometimes too severe further research in progress

- Material laws:
 - New laws for reinforcing steel "STEELEC2EN". Hot rolled or cold formed bars can be chosen (see Table 3.2a of EN 1992-1-2); class A, B or C can be chosen (see Fig. 3.3 of EN 1992-1-2).
 Note: in previous versions, cold worked, class B or C was used.
 - New types of material for high strength concrete (table 6.1N of EN 1992-1-2 for the reduction of strength with temperature): "SILHSC1ETC", "SILHSC2ETC", "SILHSC3ETC", "CALHSC1ETC", "CALHSC2ETC", "CALHSC3ETC".

- Solver, algorithms and CPU time
 - Structural calculations continue even with negative values on the main diagonal of the stiffness matrix, which gives a better insight into the **failure mode**.
 - Reduction of CPU time by approximately a factor 2 for simulations with HASEMI fires.

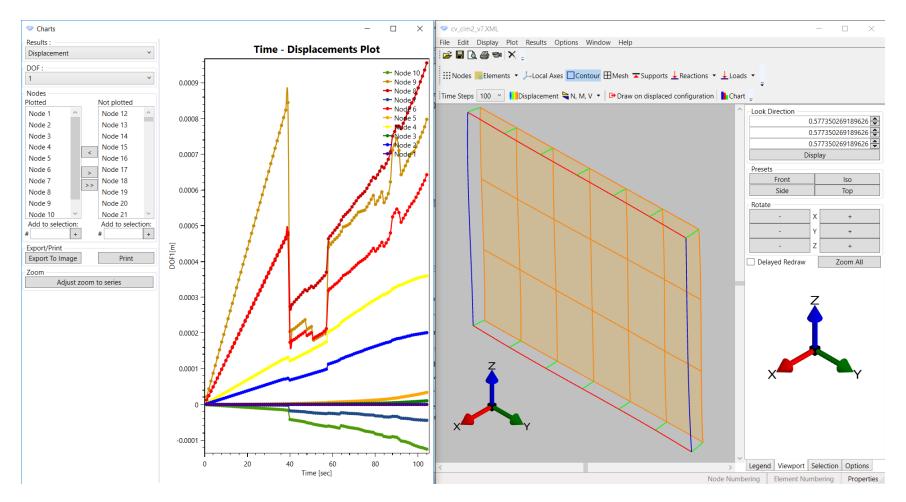
- Output files
 - Results written in an XML file in order to facilitate post-processing (see the Section about DIAMOND).

- Completely **re-written in C++**
- Based on the **XML file** produced by SAFIR (from versions 2016).

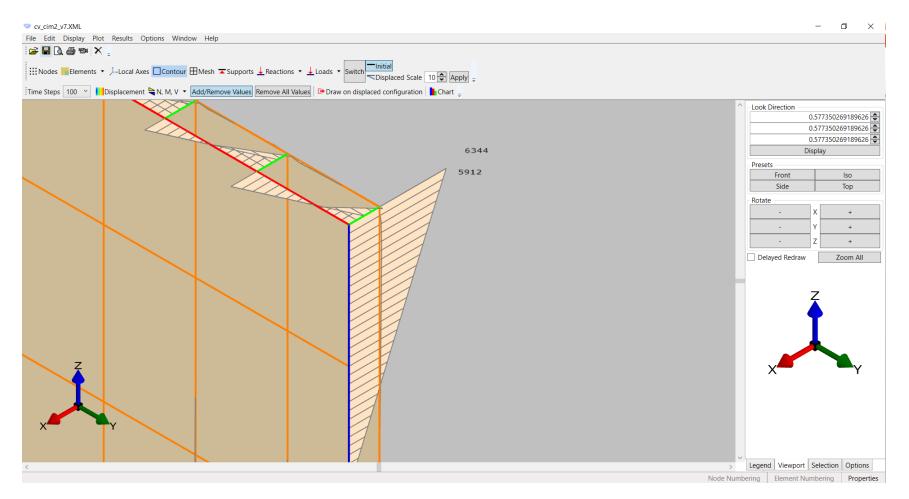
The results of this are:

- Possibility to treat larger files (was limited to 2 Gb previously);
- Much **faster** opening of the program and initial reading of the file;
- Allows to keeps several "chart" windows opened, with an unlimited number of curves in each window (was limited to 5 curves previously);
- Possibility to paint the results (M, N, V diagrams on beams, membrane or bending forces on shells, displacement colours in shells) on the displaced structure.
- Possibility to add values on the M, N, V diagrams
- ⇒ Work in progress, further developments planned (happy to hear your feedbacks)

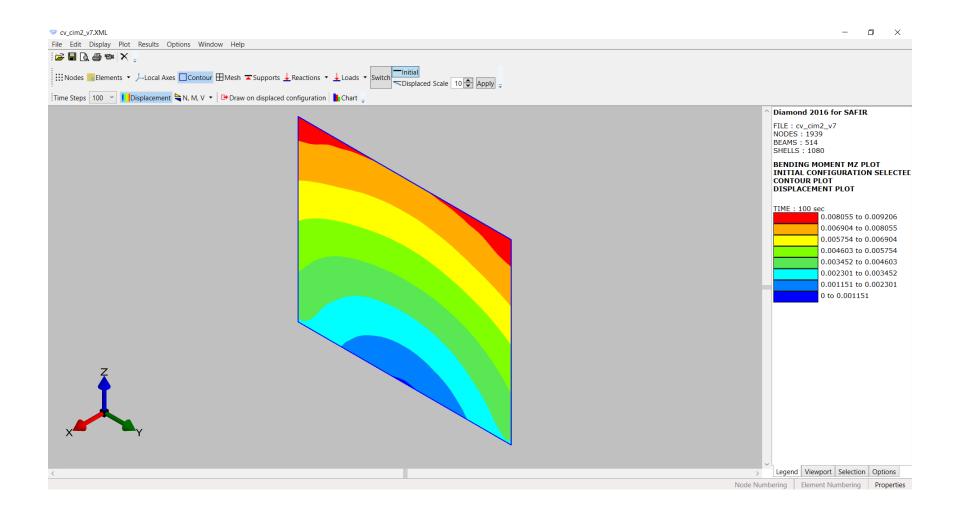
Multiple charts / curves



Peak values plotted on the M diagram



ACKNOWLEDGEMENT DEVELOPMENT OF THIS CAPABILITY SUPPORTED BY « Lenz Weber Ingenieure GmbH »



4. DISTRIBUTION AND EVOLUTION POLICY

- The problem types for GID-SAFIR interface can be downloaded for free from the SAFIR website <u>http://www.facsa.ulg.ac.be/cms/c 1629716/en/safir-free-downloads</u>; updates will be posted regularly on the website.
- The version 2016 of Diamond can be downloaded for free from the SAFIR website <u>http://www.facsa.ulg.ac.be/cms/c_1629716/en/safir-free-downloads</u>; updates will be posted regularly on the website. Note that it requires the version of SAFIR 2016 or later to work, because it needs the XML output file produced by these versions.
- The previous version of Diamond, the one that reads the .OUT file will still be available for download on the SAFIR website, but it will not be developed nor maintained in the future.
- The new versions of SAFIR will still produce an .OUT file in parallel to the XML file, but this .OUT file is for your eyes utilisation. It is not anymore intended to be used by Diamond 2016.
- Free updates are normally granted for one year after acquisition of a licence. The new version of the SAFIR executable will be delivered for free to any user who acquired a licence on or later than January 1^{rst}, 2015.
- Users who acquired their licence before 2015 can acquire an update for 1 000 € (commercial licence) or 250 € (academic licence). If interested, please contact <u>safir@ulg.ac.be</u> to obtain a coupon that will allow buying at a discount price on http://www.gesval.be/en/catalogue/safir-commercial (commercial) or http://www.gesval.be/en/catalogue/safir-commercial (academic).

5. REFERENCES

The references to be quoted when using SAFIR are:

- Franssen, J.M., Gernay, T. (in press). "Modeling Structures in Fire with SAFIR[®]: Theoretical Background and Capabilities", *Journal of Structural Fire Engineering*.
- Franssen, J.M. (2005). "SAFIR. A Thermal/Structural Program Modelling Structures under Fire", Engineering Journal, A.I.S.C., Vol 42, No. 3, 143-158. <u>http://hdl.handle.net/2268/2928</u>
- Please also quote the adequate references when using the material models CALCON_ETC, SILCON_ETC, STEELSL, CALCOETC2D, CALCOETC3D, etc. (references specified in the Users manual of SAFIR 2016 – mechanical).

QUESTIONS

For questions about the SAFIR suite, please write us as at <u>safir@ulg.ac.be</u> with copy to:

- Installation of the software and administrative questions: <u>a.scifo@ulg.ac.be</u>
- GiD and DIAMOND: jdferreira@ulg.ac.be
- SAFIR: <u>jm.franssen@ulg.ac.be</u> and <u>thomas.gernay@ulg.ac.be</u>