

Modeling and analysis of nonlinear systems applied to a guitar signal chain.

ABAV, Sart-Tilman, Feb 21

SCHMITZ Thomas

Department of Electrical Engineering and Computer Science,
University of Liège

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Introduction to the
guitar instrumentation
problem

Non-linear modelling
IR measurement
Model reconstruction

Non-linear loudspeaker
simulation

Objective evaluation
of the model

Subjective evaluation
of the model

Conclusion

Communication Outline



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- IR measurement

- Model reconstruction

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Section 1

Introduction to the guitar instrumentation problem

Goals of the thesis

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FIGURE: A guitar chain example



FIGURE: Objective of the work

Utility ?



FIGURE: Home studio ?



FIGURE: Home studio !

Advantages of the simulation :

- ▶ Wide variety of sounds and timbres.
- ▶ Weight and overcrowding.
- ▶ Easier comparison between two sounds.
- ▶ Cheaper.

Disadvantages of the simulation :

- ▶ Fidelity of the sound \Rightarrow accuracy of the model.
- ▶ Psychologic :
 - ▶ An emulation still be an emulation.
 - ▶ Numerical sounds is cooler than analogical sound.

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Section 2

Non-linear modelling

Non-linear modelisation : Black box approach



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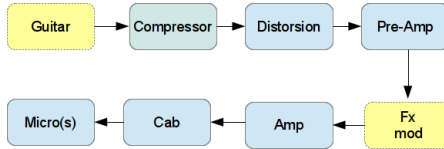


FIGURE: Guitar chain,in blue the non-linear elements

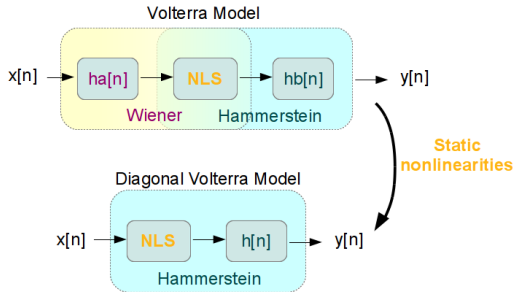


FIGURE: Nonlinears models

Non-linear modelisation : Volterra Series



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Relation between input $x[n]$ and output $y[n]$ for non-linear system

$$\left\{ \begin{array}{l} y[n] = \sum_{i=1}^M \sum_{\tau_1=0}^N \dots \sum_{\tau_i=0}^N h_i[\tau_1, \dots, \tau_i] x[n - \tau_1] \dots x[n - \tau_i] \end{array} \right. \quad (1)$$

Where $h_i[n]$ If the non-linearities are static, then

$h_i[\tau_1, \dots, \tau_i] = 0 \quad \forall \tau_k \neq \tau_1 \text{ with } k \in [1, i]$.

Ex 2th Volterra kernel :

$$\begin{pmatrix} 1 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0.9 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0.8 & 0 & \dots & 0 \\ \vdots & \ddots & & & & \\ \dots & & & & 0 & 0.1 \end{pmatrix}$$

Eq (1) becomes :

$$y[n] = x[n] \otimes h_1[n] + x[n]^2 \otimes h_2[n] + \dots + x[n]^M \otimes h_M[n] \quad (2)$$

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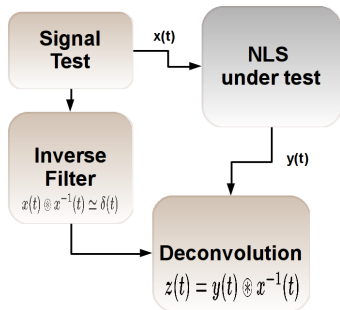


FIGURE: Impulse response measurement.

We choose :

$$x(t) = A \sin(\varphi(t)) \quad (3)$$

where the variable phase $\varphi(t)$ grows exponentially. This property allows us to separate the different orders of distortion as (for example) :

$$x^3(t) = \frac{A^3}{4} [3 \sin(\varphi(t)) - \sin(3\varphi(t))] \quad (4)$$

We can show that it exist a link between :

$$M.\varphi(t) \Leftrightarrow \varphi(t + \Delta_M) \quad (5)$$

So that

$$x^3(t) \otimes x^{-1}(t) \Rightarrow \delta(t) + \delta(t + \Delta_3) \quad (6)$$

Deconvolved signal



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$$\begin{aligned} z[n] &= y[n] \otimes x^{-1}[n] \\ &= \left(x[n] \otimes h_1[n] + x[n]^2 \otimes h_2[n] + \dots + x[n]^M \otimes h_M[n] \right) \otimes x^{-1}[n] \end{aligned} \quad (7)$$

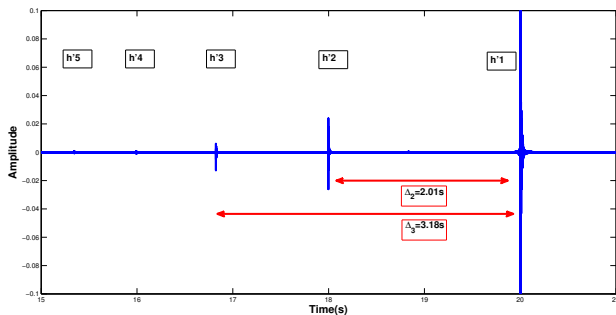


FIGURE: Impulse response measurement. $z(t)$ the deconvolved signal

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Connection between Volterra kernels h_i and measured kernels m_i



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We have proved :

$$\mathcal{F}(h_i) \xleftrightarrow{\text{link}} \mathcal{F}(m_i)$$

So that, we obtain ($\forall \omega > 0$) :

$$\mathcal{F}(h_i) \iff \mathcal{F}(m_i)$$

$$\left\{ \begin{array}{l} H_1(w) = M_1(w) + 3e^{2jB} M_3(w) + 5e^{4jB} M_5(w) \\ H_2(w) = \frac{2}{A} j e^{jB} [M_2(w) + 4e^{2jB} M_4(w)] \\ H_3(w) = \frac{-4}{A^2} e^{2jB} [M_3(w) + 5e^{2jB} M_5(w)] \\ H_4(w) = \frac{8}{A^3} (-j e^{3jB}) M_4(w) \\ H_5(w) = \frac{16}{A^4} M_5(w) e^{4jB} \end{array} \right. \quad (8)$$

Where A takes into account of the amplitude of the emitted sine sweep and B depends on the parameters of the chosen sweep

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Non-linear loudspeaker simulation

Comparison between the real and simulated signal

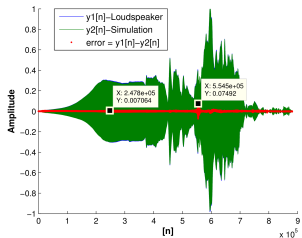


FIGURE: Simulation with 5 Volterra kernels

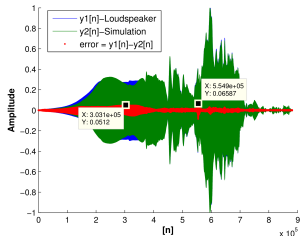
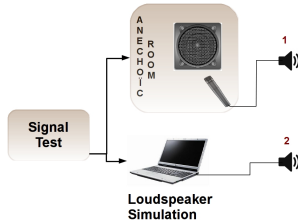


FIGURE: Simulation with 1 Volterra kernel

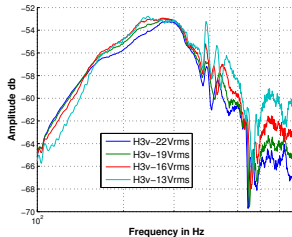
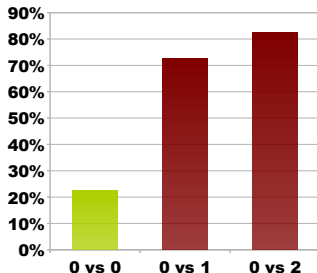


FIGURE: $H_3(\omega, \text{Amplitude})$

Compare sample 0 to samples 0, 1, 2

% of error



Sample 0 : Real

**Sample 1 : Simulated
With 1 Volterra kernel**

**Sample 2 : Simulated
With 5 Volterra kernels**

FIGURE: 82% of tested listener were not able to distinguish a simulation of type 2. 72% of tested listener were not able to distinguish a simulation of type 1 and 22% of tested listener hear a difference where there were none !

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Section 4

Conclusion

Achievement

- ▶ Non-linear loudspeaker modelisation based on Volterra series.
- ▶ Subjective and objective evaluation of the model.

Future works

- ▶ Improve *simulation* fidelity.
- ▶ Solving the amplitude dependance of the model.
- ▶ Try the model on more non-linear system.

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Thank you for your attention !