

Power system dynamic simulation: an iterative multirate approach

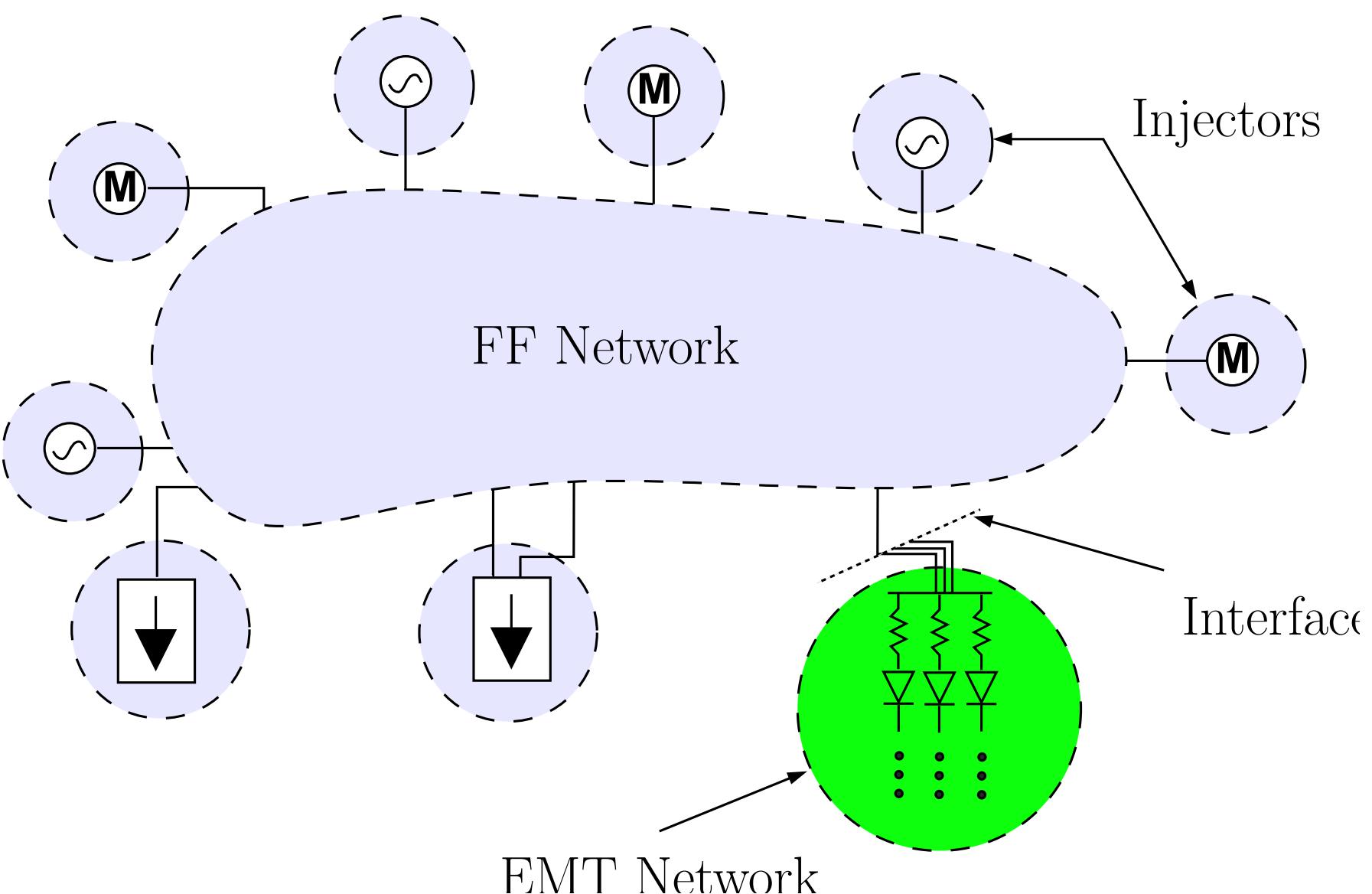
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Objective: Combine accuracy of detailed EMT simulation with efficiency of simplified FF simulation.

1. Power System representation



In dynamic simulations, power system components are modeled by sets of *nonlinear stiff hybrid Differential-Algebraic Equations* (DAEs).

The i -th injector can be described by a DAE system of the form:

$$\Gamma_i \dot{\mathbf{x}}_i = \Phi_i(\mathbf{x}_i, \mathbf{V})$$

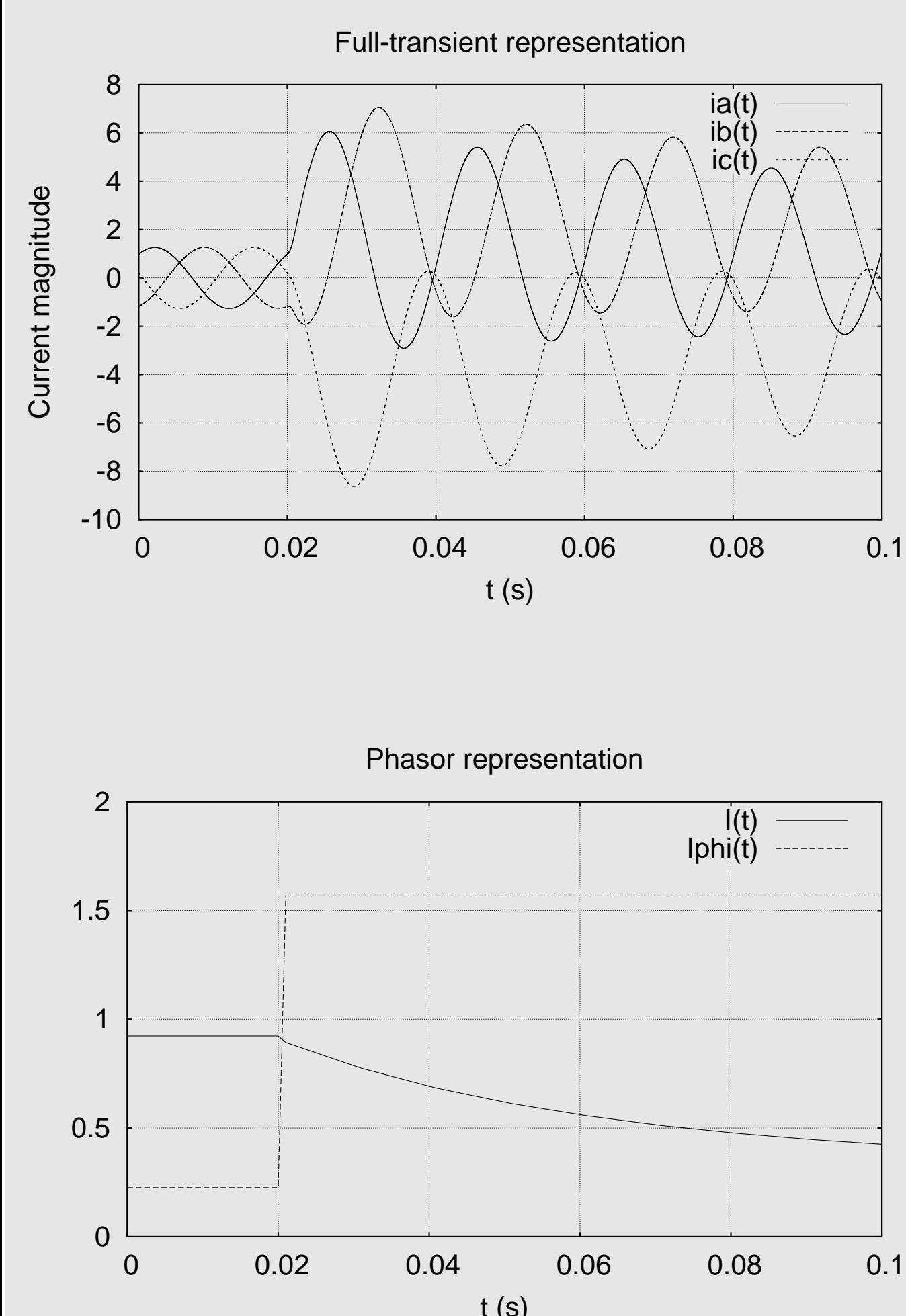
where \mathbf{x}_i the model's internal states, $\bar{V}_{k+1}^{(j)}$ ($(\Gamma_i)_{\ell\ell} = \begin{cases} 0 & \text{if the } \ell\text{-th equation is algebraic} \\ 1 & \text{if the } \ell\text{-th equation is differential} \end{cases}$) and \mathbf{V} the vector of network voltages.

Two modeling families are traditionally used in power system dynamic simulations:

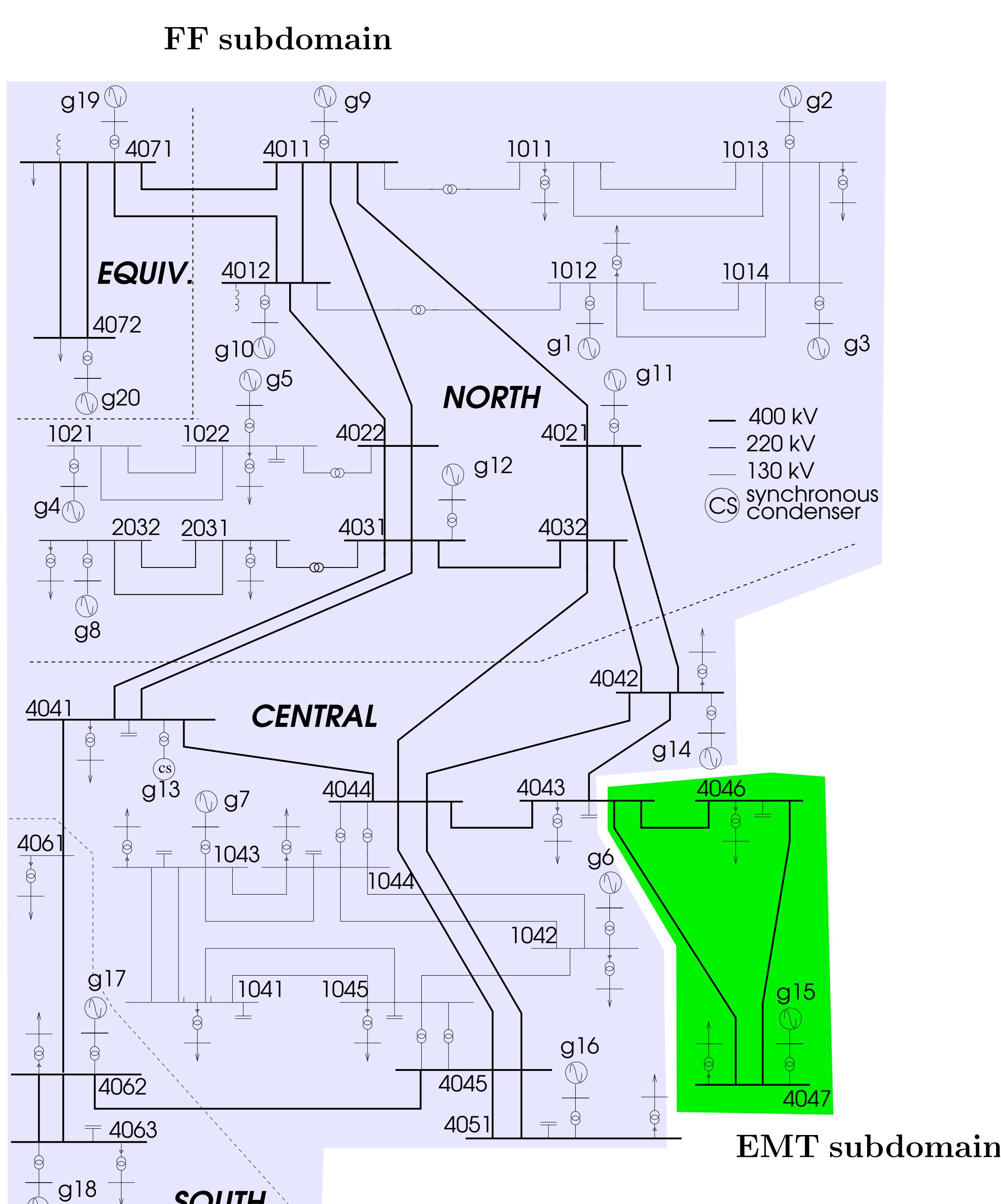
1. Full-Transient or ElectroMagnetic Transients (EMT) simulation
2. Fundamental-Frequency (FF) approximation for which the network can be described by the linear algebraic equations:

$$0 = DV - I = g(x, V)$$

EMT vs FF: Three-phase fault

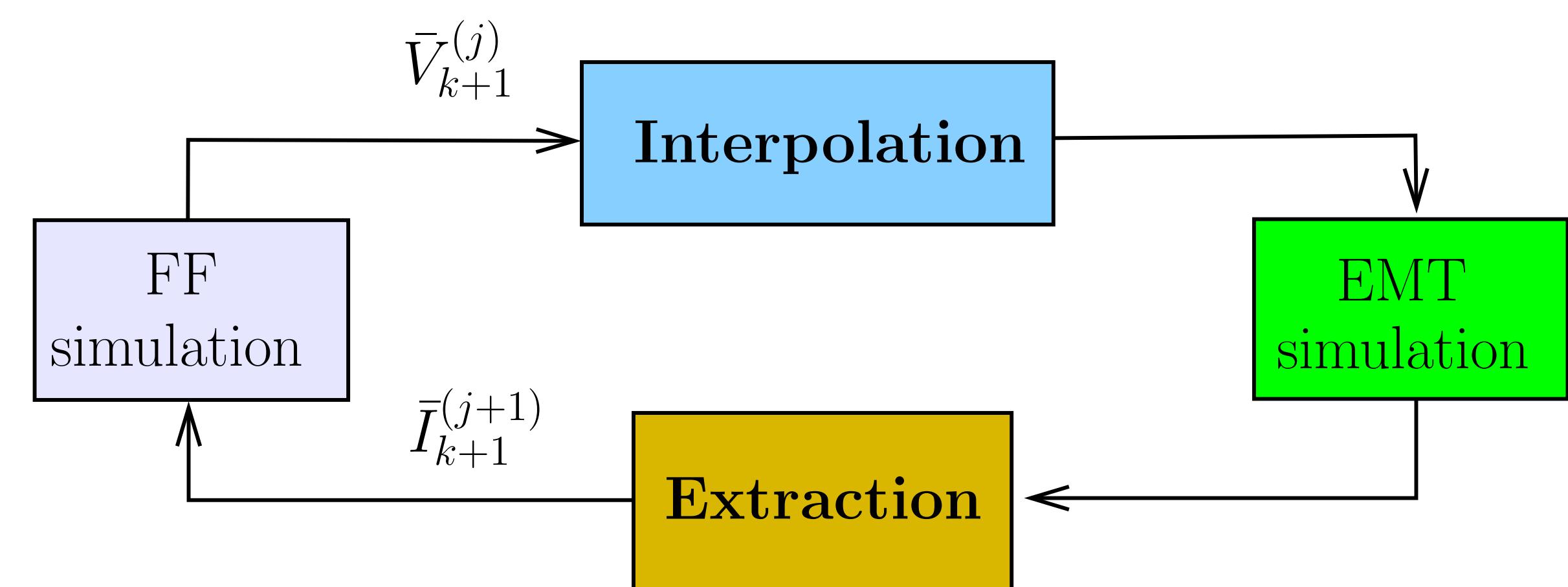


3. Test system: Nordic-32

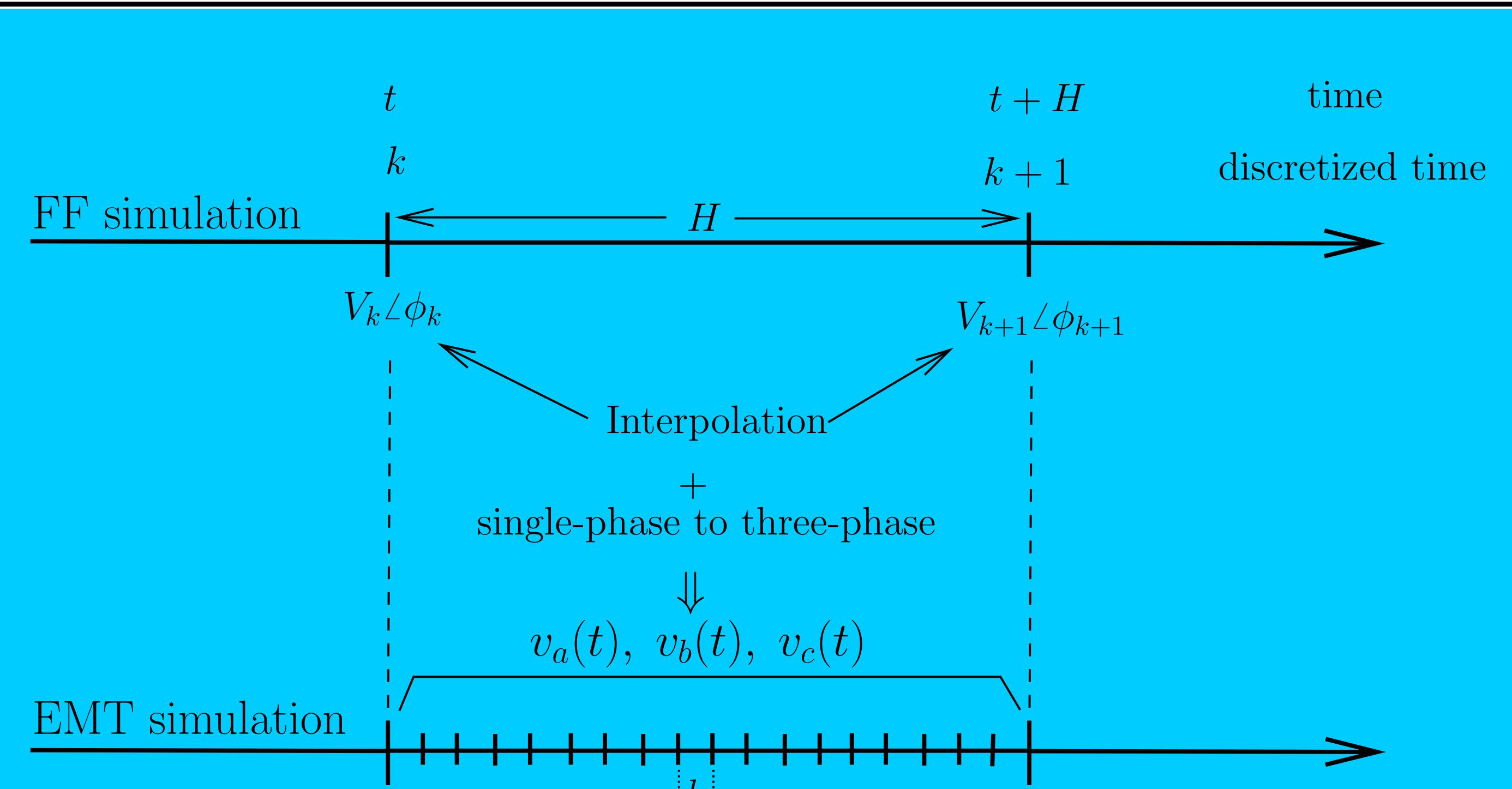


2. Iterative multirate approach

Gauss-Seidel relaxation until convergence



Interpolation



Considering phase a , for instance, the voltage evolution is taken as ($n = 0, 1, 2, \dots$):

$$v_a(t+nh) = \sqrt{2} V_a(t+nh) \cos(\omega(t+nh) + \phi_a(t+nh))$$

where $V_a(t+nh) = V_a(t) + (V_a(t+H) - V_a(t)) \cdot \frac{nh}{H}$

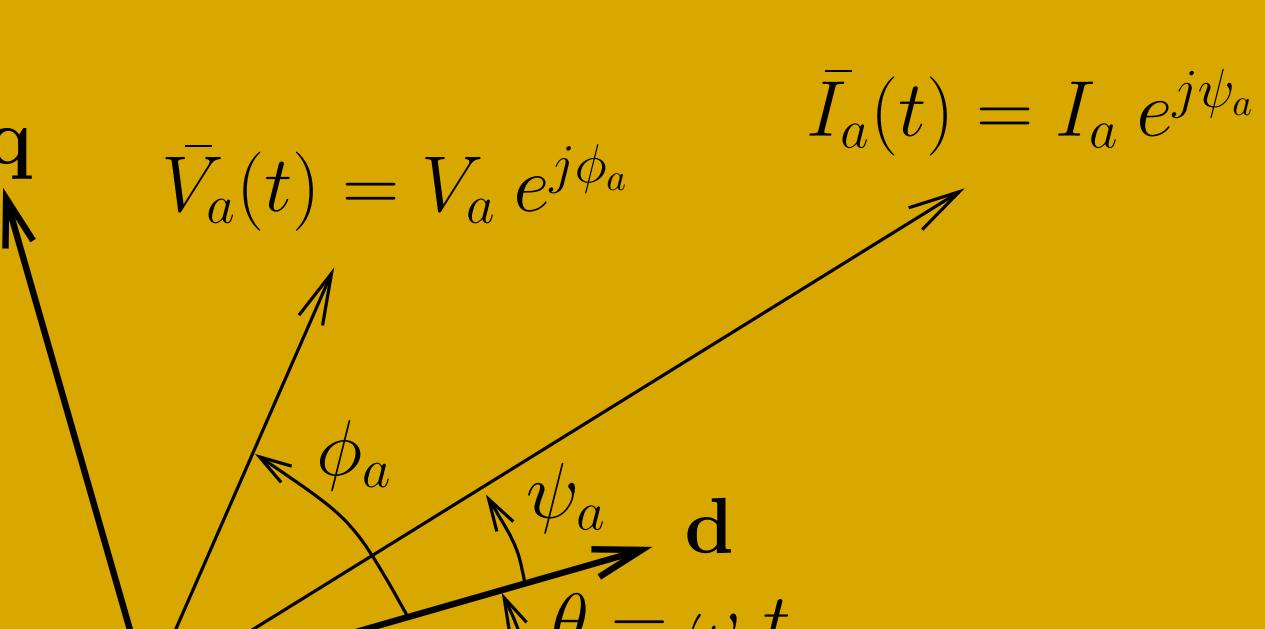
and $\phi_a(t+nh) = \phi_a(t) + (\phi_a(t+H) - \phi_a(t)) \cdot \frac{nh}{H}$

where ω is the nominal angular speed of the system.

Extraction: projection on a rotating frame + filtering

$$\mathbf{I}_{0qd} = \mathbf{T} \mathbf{I}_{abc} = \frac{\sqrt{2}}{3} \begin{bmatrix} 1/\sqrt{2} & 1/\sqrt{2} & 1/\sqrt{2} \\ \cos(\theta) & \cos(\theta - \frac{2\pi}{3}) & \cos(\theta - \frac{4\pi}{3}) \\ -\sin(\theta) & -\sin(\theta - \frac{2\pi}{3}) & -\sin(\theta - \frac{4\pi}{3}) \end{bmatrix} \begin{bmatrix} i_a(t) \\ i_b(t) \\ i_c(t) \end{bmatrix} \approx \begin{bmatrix} 0 \\ I_a \cos \psi_a \\ I_a \sin \psi_a \end{bmatrix}$$

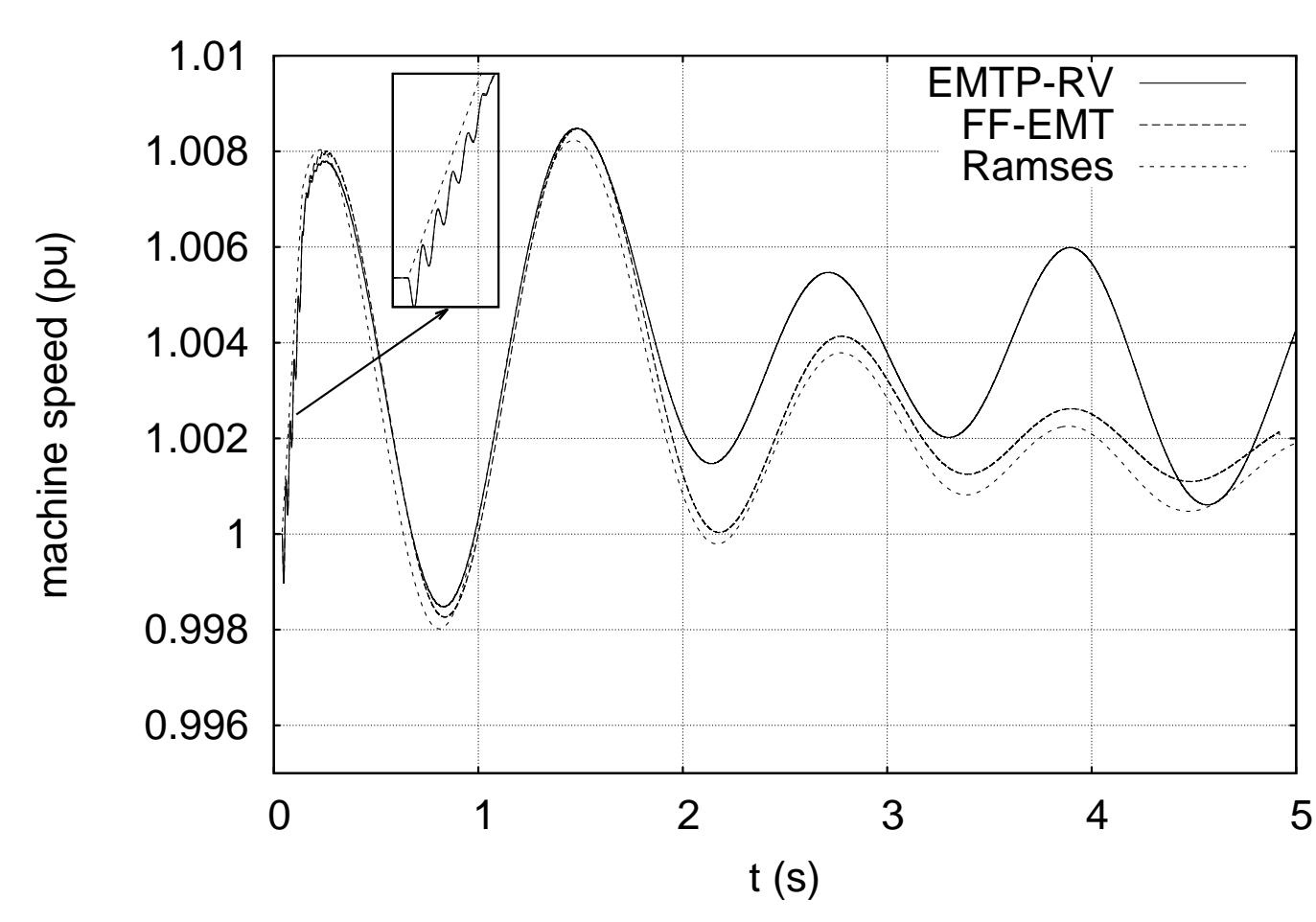
$\bar{I}_a(t) = I_a e^{j\psi_a}$

$$\Rightarrow I_a = \sqrt{I_d^2 + I_q^2} \quad \psi_a = \arctan\left(\frac{I_q}{I_d}\right)$$


The diagram shows the transformation from a three-phase frame (a, b, c) to a rotating frame (d, q). The voltage $\bar{V}_a(t) = V_a e^{j\phi_a}$ is converted to $\bar{I}_a(t) = I_a e^{j\psi_a}$ using the transformation matrix. The current I_a is then calculated as the magnitude of the transformed current, and the angle ψ_a is determined from the ratio of the q and d components.

4. Preliminary results for a three-phase fault

Rotor speed of machine g15



Voltage at bus 4043

