

# Numerical simulations of the sound propagation in non rectilinear streets

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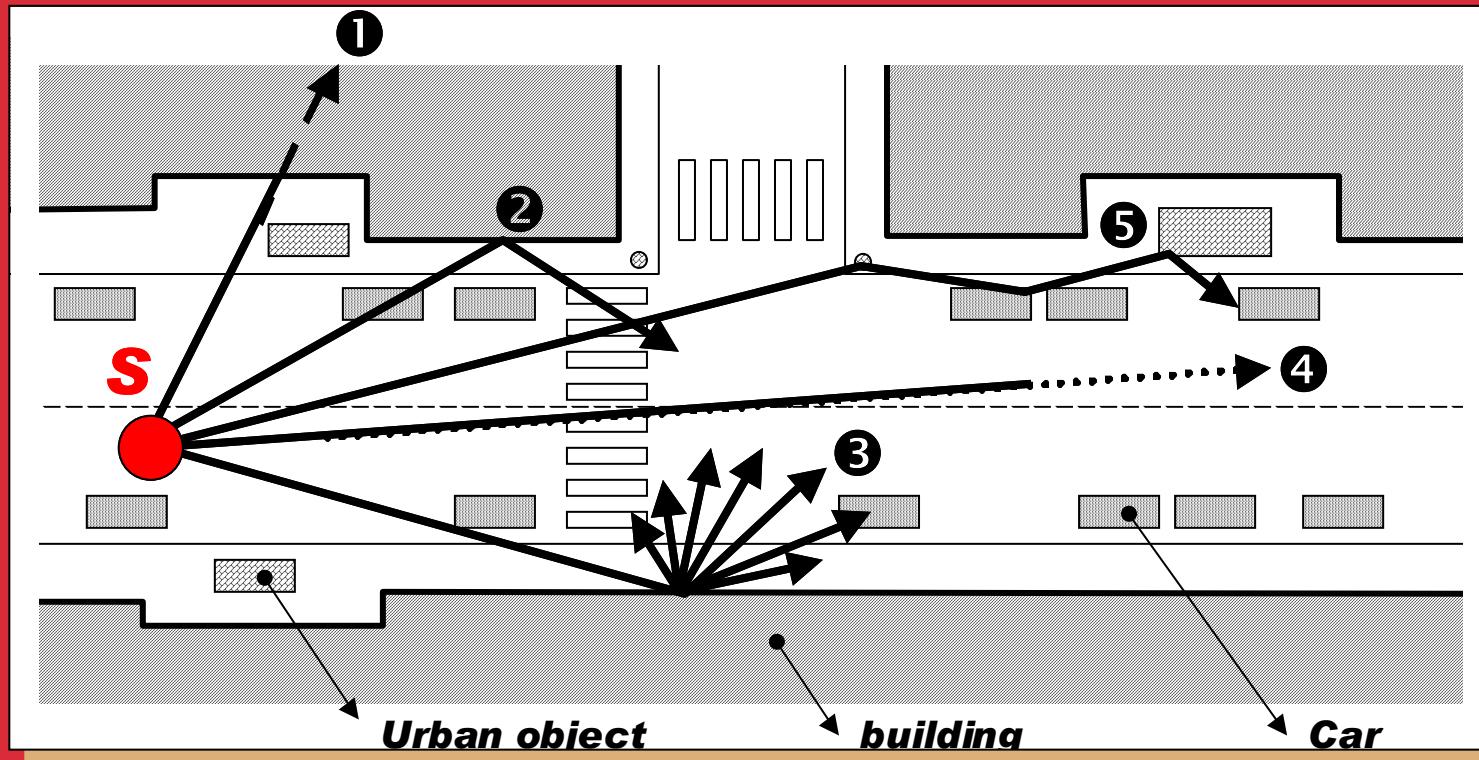
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# 1. Introduction



- Integrating all these physical phenomena;
- Minimizing the computation time;
- Dealing with complex geometries.
- Comparison of ray-tracing's and diffusion model's results and experiments on scale models for non-rectilinear streets

# 2. Models presentation

- Diffusion model

- Starting with the motion of sound particles
- Using an asymptotic development (Le Pollès, 2003)

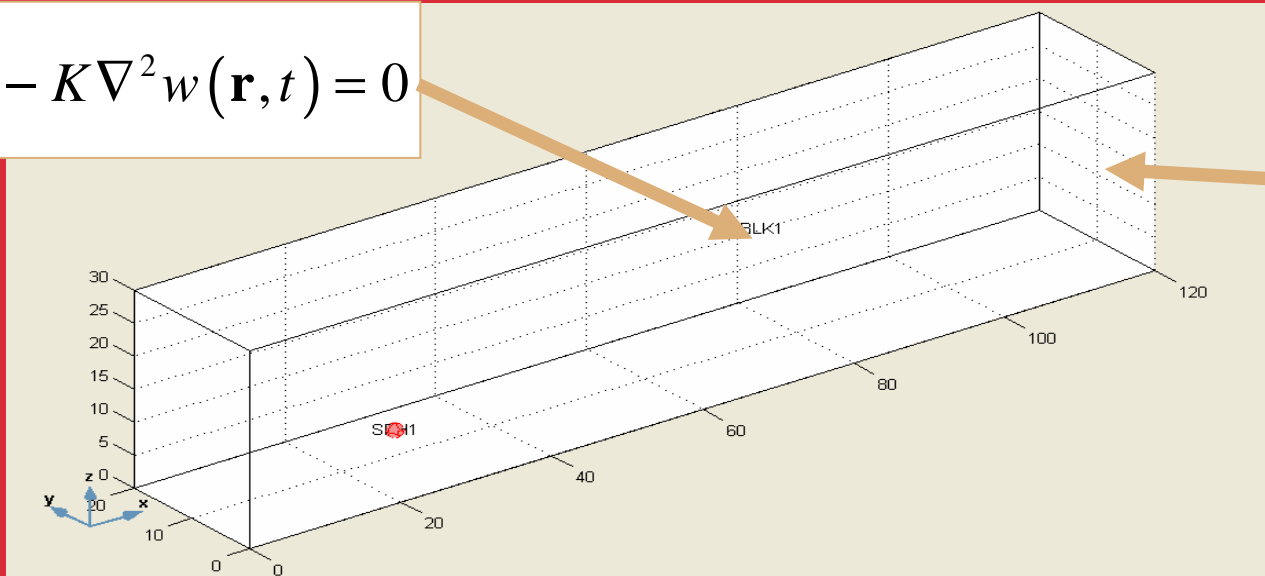
Transport equation



Diffusion equation

- Solving using finite elements (Colle, 2006)

$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - K \nabla^2 w(\mathbf{r}, t) = 0$$



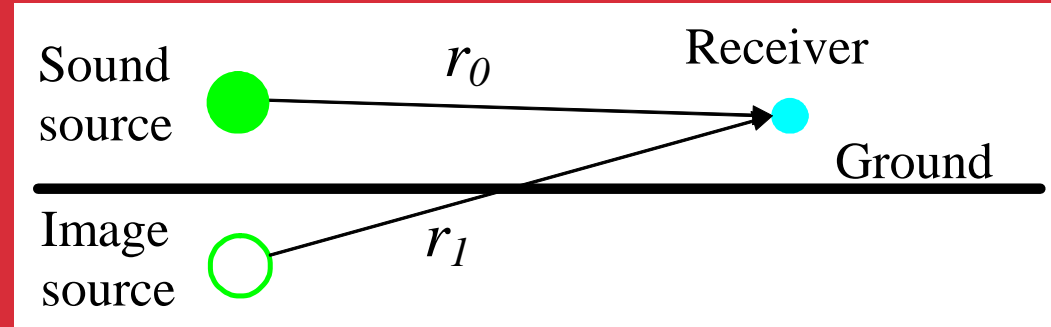
$$h = \frac{c}{2} \alpha$$

$$K = \frac{2 - s}{s} \frac{\ell c}{2}$$

$\ell$  street half-width  
 $s$  scattering coefficient  
 $c$  sound speed

## 2. Models presentation

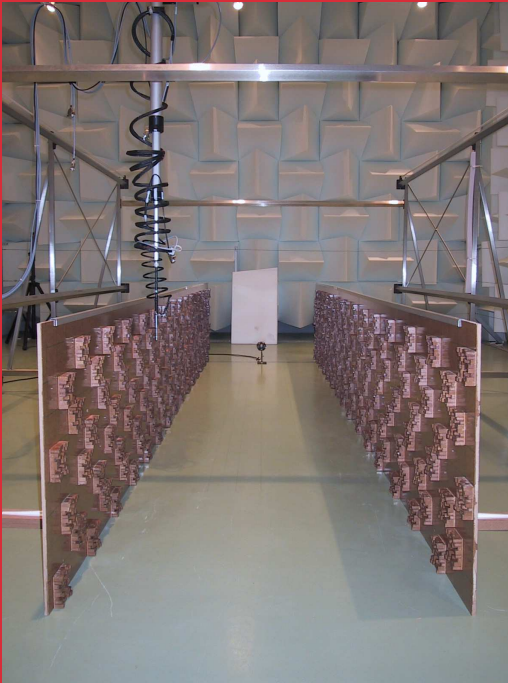
- Sound pressure level



$$SPL(\mathbf{r}) = 10 \log_{10} \left[ \frac{\rho c}{p_{ref}^2} \left( \frac{W_s}{4\pi r_0^2} + (1 - \alpha_s) \frac{W_s}{4\pi r_1^2} + cw(\mathbf{r}) \right) \right]$$

- Good agreement in terms of SPL with numerical and experimental results for rectilinear streets
- Inability to predict sound decay (Billon & Picaut, 2008)
- Broadband ray-tracing Salrev (Embrechts, 2000)

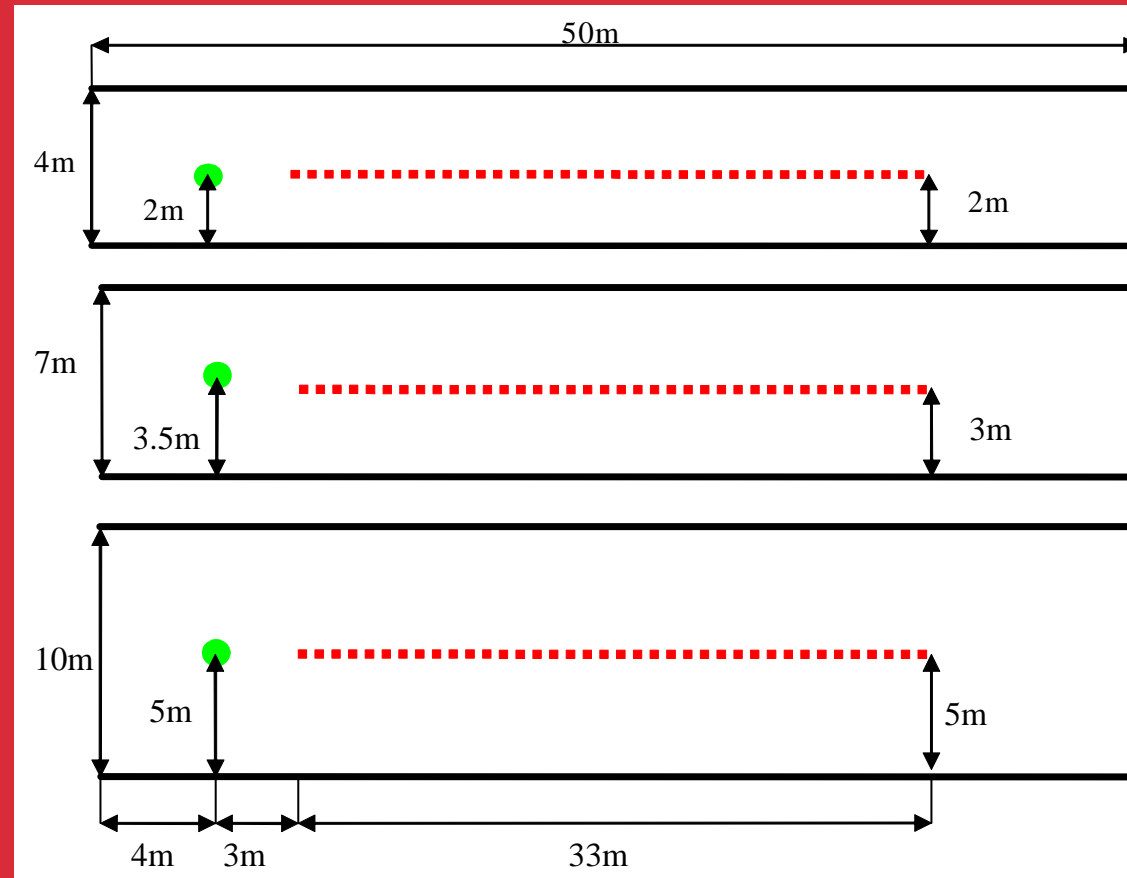
## 3. Experimental apparatus



- Scale 1/10<sup>th</sup>
- Ø 65 mm dodecahedric sound source
- 1/4" free field microphone
- Varnished plywood fitted with sound diffusors
- Measurements between 100 Hz and 8 kHz (full scale)
- Atmospheric attenuation compensated with a time-varying filter
- Evaluation of SPL and reverberation times (RT10)

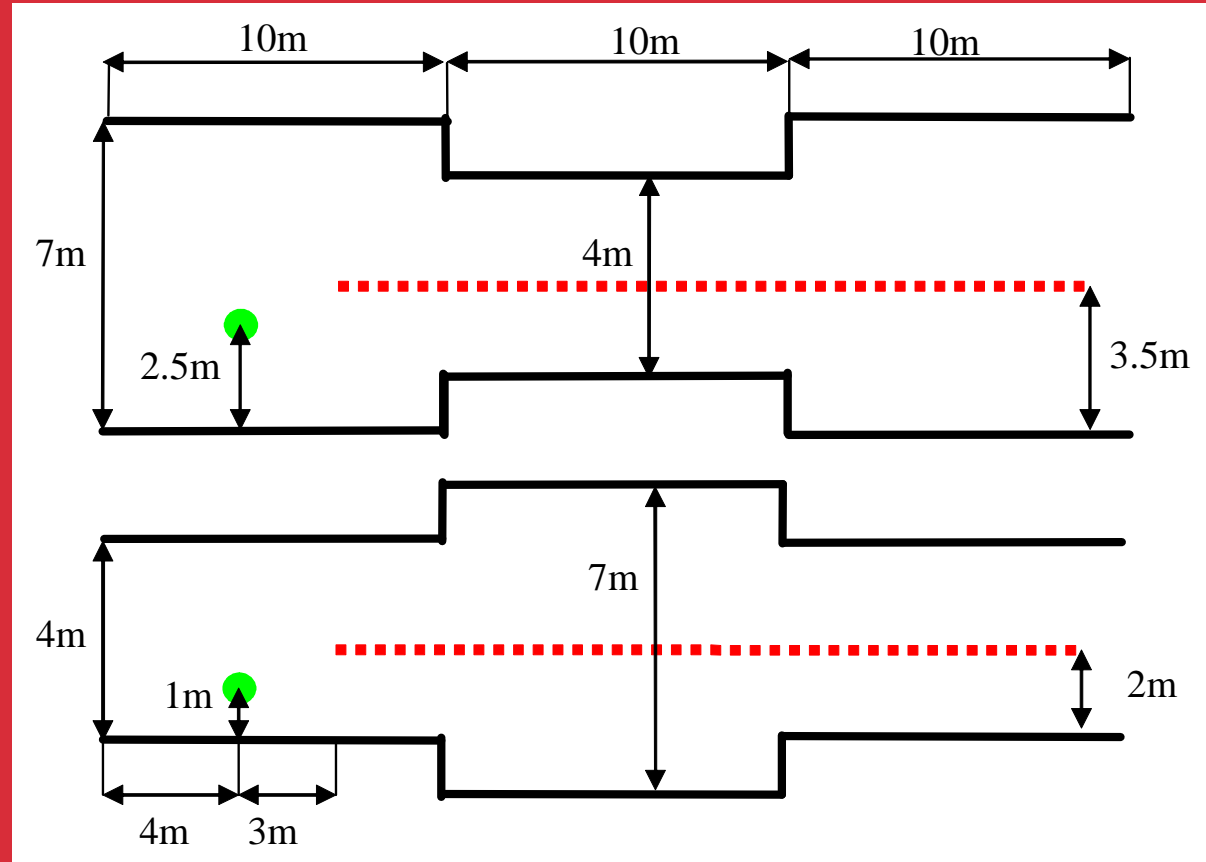
# 3. Experimental apparatus

- Tree straight configurations



# 3. Experimental apparatus

- Two configurations with varying cross-section







# 4. Numerical parameters

- Ray-tracing
  - Ø 1 m sound receivers
  - $10^8$  rays
  - Computation time 1h~1h30
- Diffusion model
  - $10^4$  Lagrange linear elements
  - Computation time < 20 s
- 630 Hz third octave band (full scale)
- Boundary conditions evaluated from the rectilinear configurations

	Configuration 1 (width 4m)	Configuration 2 (width 7m)	Configuration 3 (width 10m)
$\alpha$	0.16	0.07	0.02
$s$	0.55	0.5	0.65
Mean error on SPL	1.1 dB	1.0 dB	1.1 dB
Mean error on RT	6.0%	6.9%	8.8%

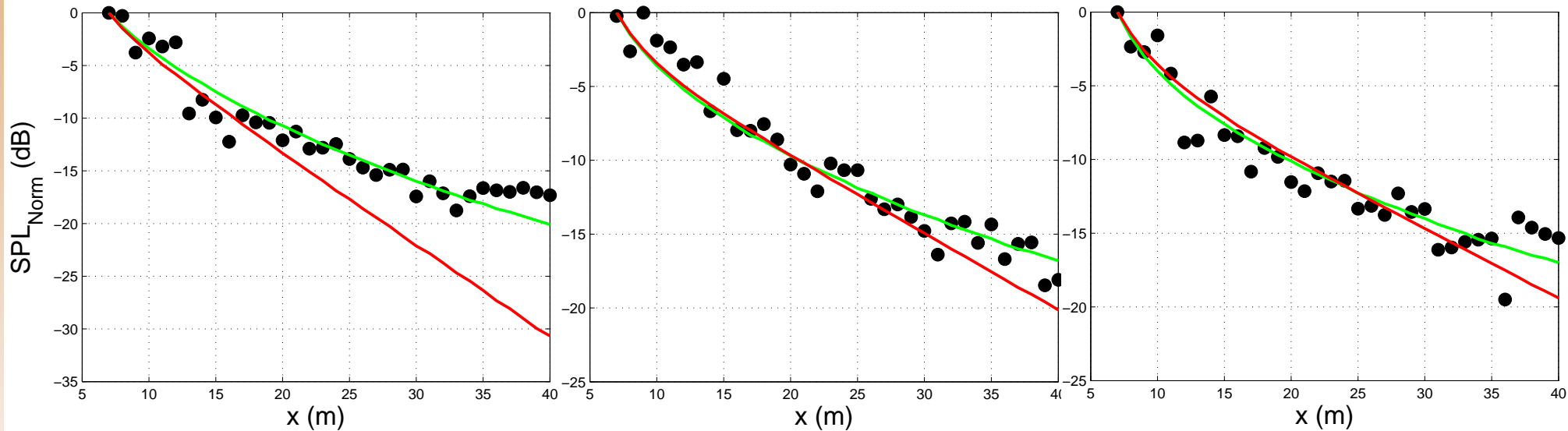
# 5. Results

## ■ Straight streets

Width 4 m

Width 7 m

Width 10 m



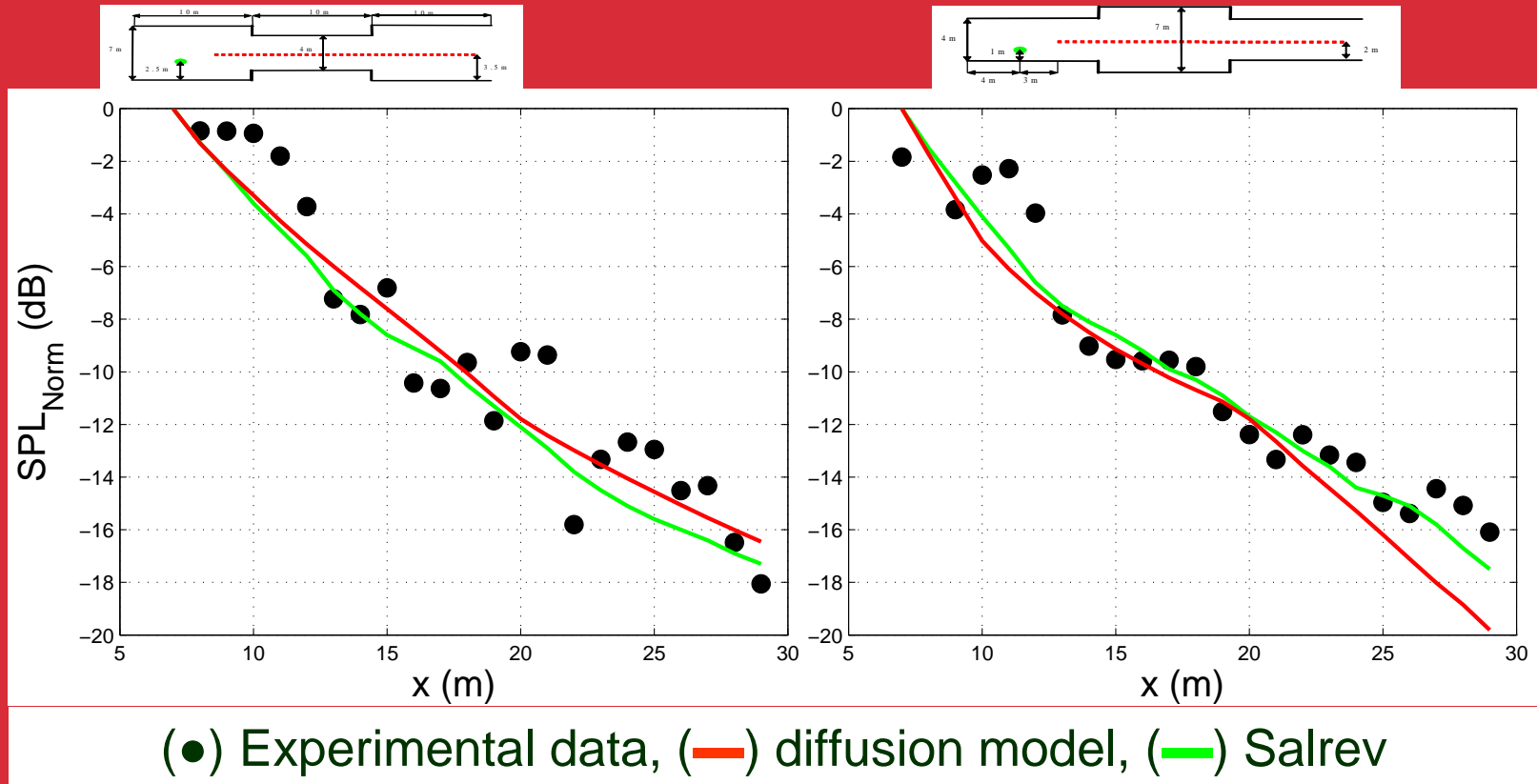
(●) Experimental data, (—) diffusion model, (—) Salrev

- Good agreement for the 7 and 10 m streets
- The diffusion model is inaccurate for the 4 m wide street

	MD	Sr
4 m	4.1	1.1
7 m	1.3	1.0
10 m	1.4	1.1
Mean error (dB)		

# 5. Results

## Streets with varying cross-section



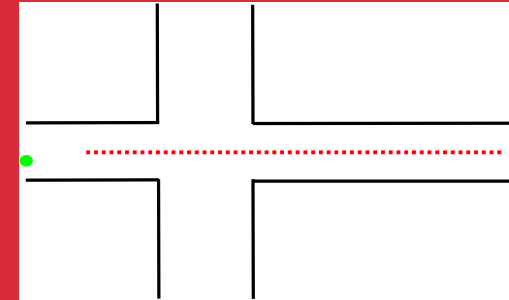
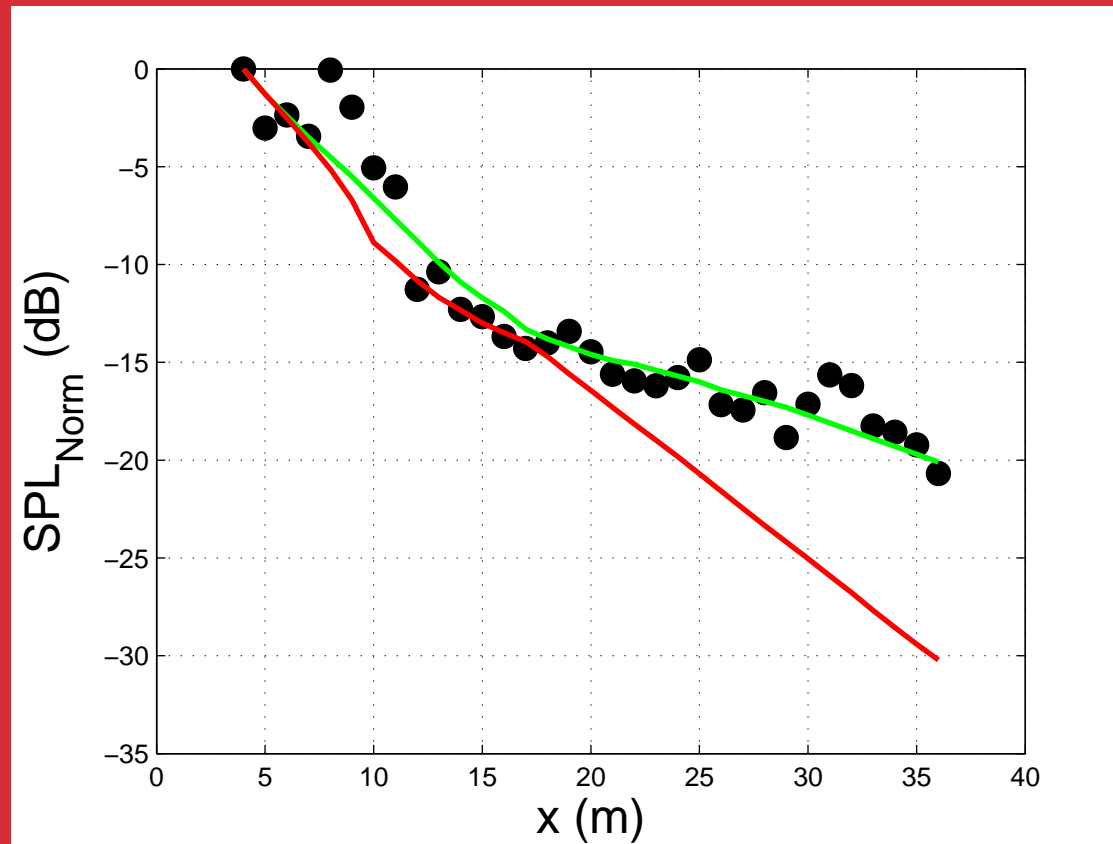
## Good agreement for both models

	MD	Sr
1	1.4	1.5
2	1.6	1.1

Mean error (dB)

# 5. Results

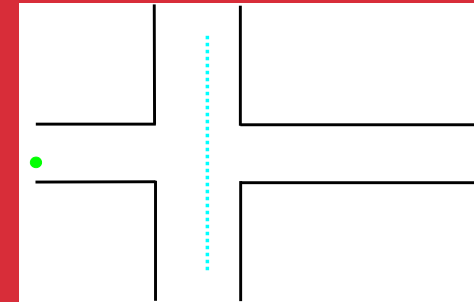
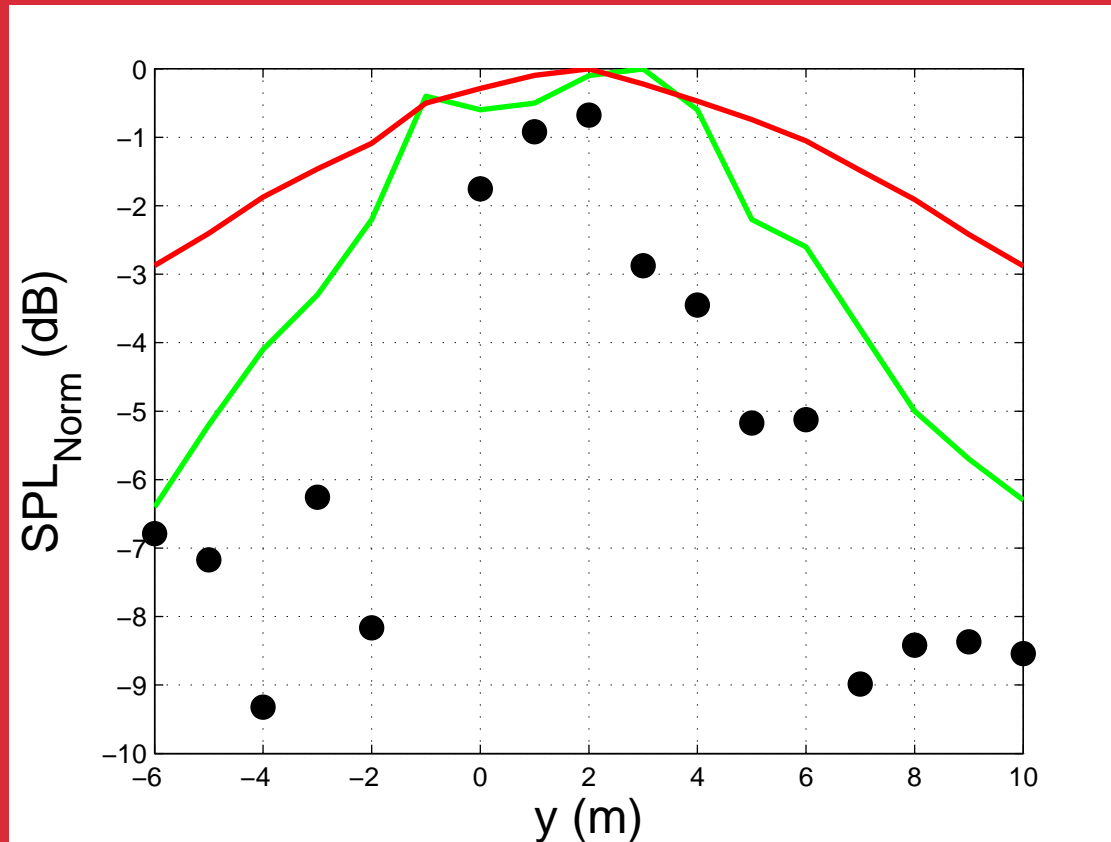
## ■ Intersection



- Good agreement for Salrev (1.1 dB)
- The diffusion model overestimates the sound attenuation in the last section

# 5. Results

## ■ Intersection



- Fair agreement for Salrev (2.6 dB)
- The diffusion model overestimates the energy flowing through the side streets

## 6. Conclusions

- Experiments on scale models have been carried out on various geometries
- Scattering and absorption coefficients have been deduced from the rectilinear streets' results
- Simulations have been made using the diffusion model and Salrev
- Salrev gives good results with a mean discrepancy around 1 dB
- The diffusion model's results are unrealistic around street corner, neglecting the directionality of the reverberant sound field

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